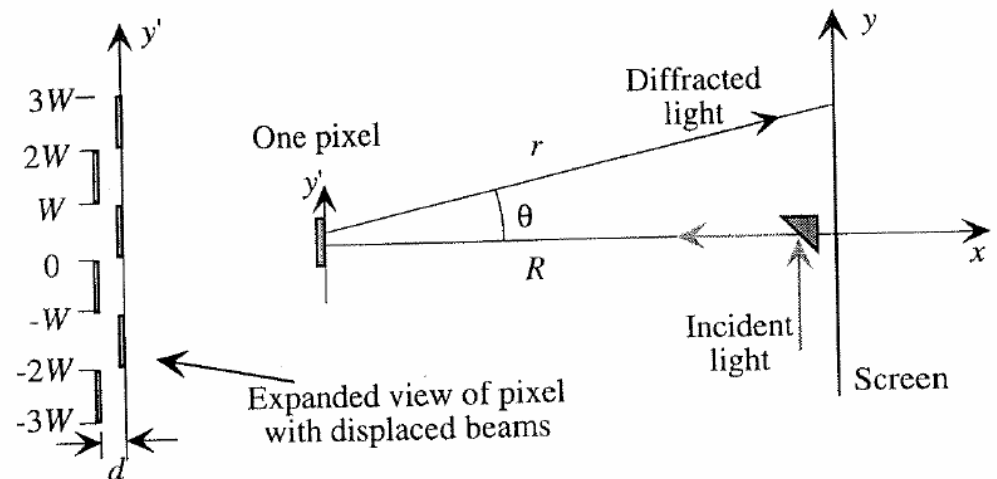
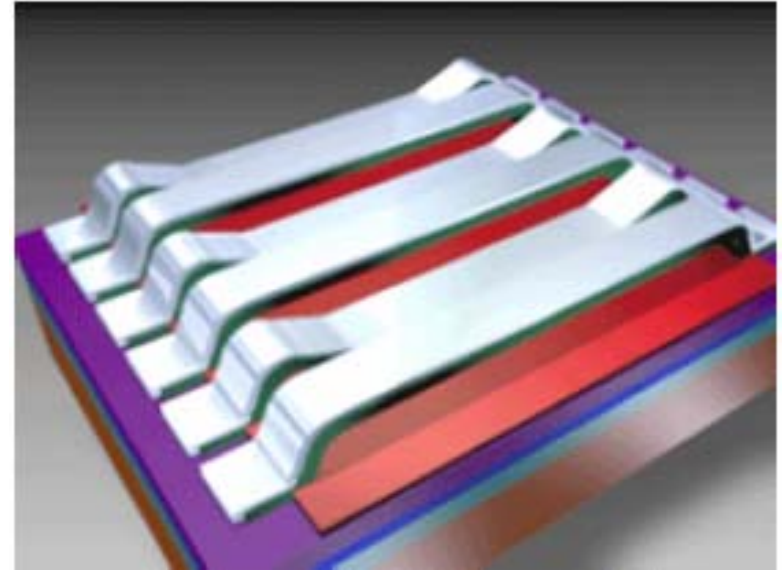


The Optics of Grating Light Valves

FYS4230

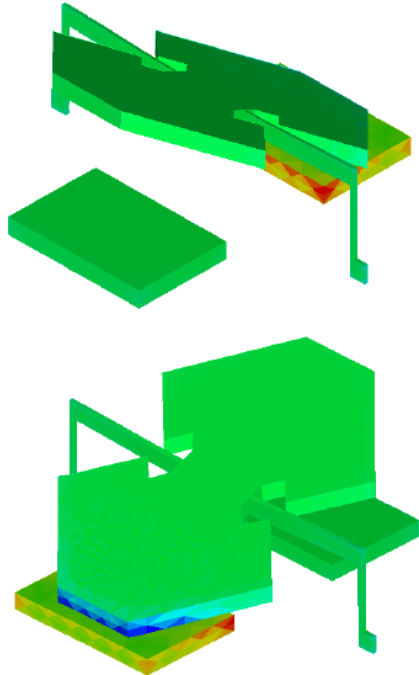
Håkon Sagberg, SINTEF



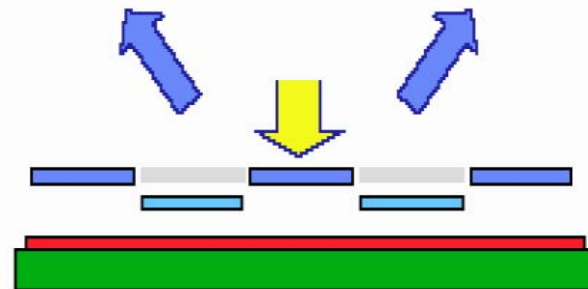
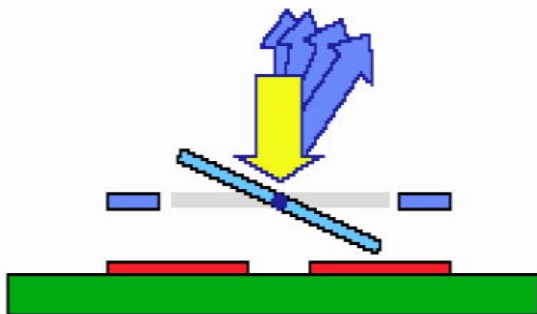
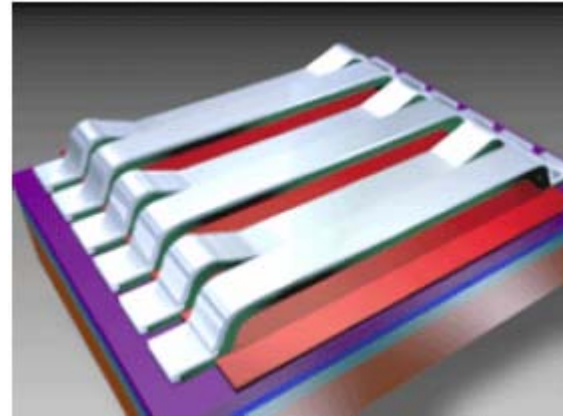
The Optics of Grating Light Valves

- Introduction to "Grating Light Valves"
- Crash course in optical diffraction theory
- The grating light valve (GLV) display
- Grating light valves for other applications
 - Spectroscopy
 - Displacement sensing

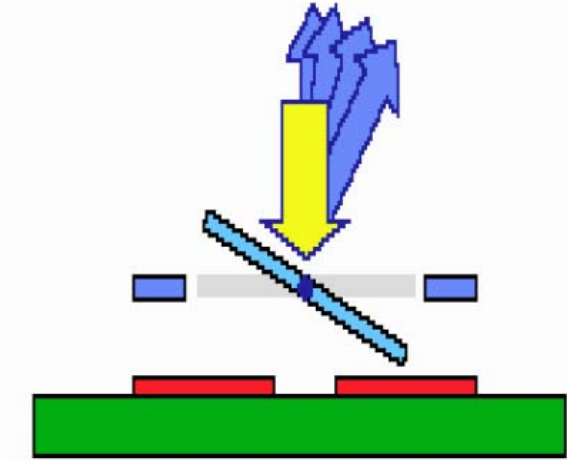
Deformable Mirror Device (DMD)



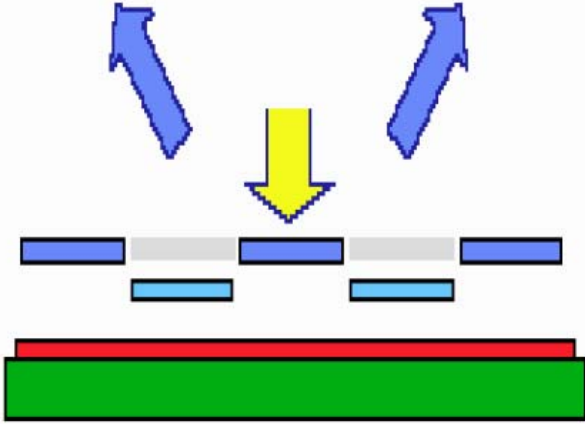
Grating light valves (GLV)



Two methods for steering light



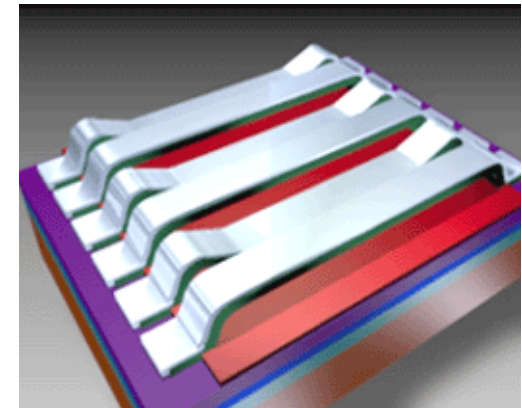
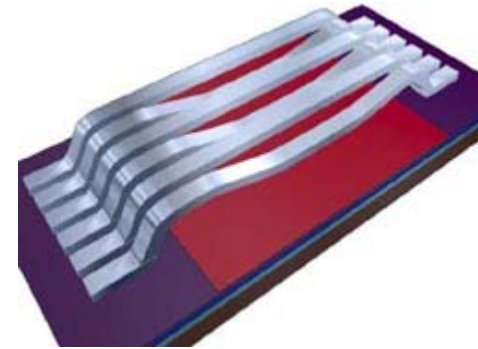
Deflection



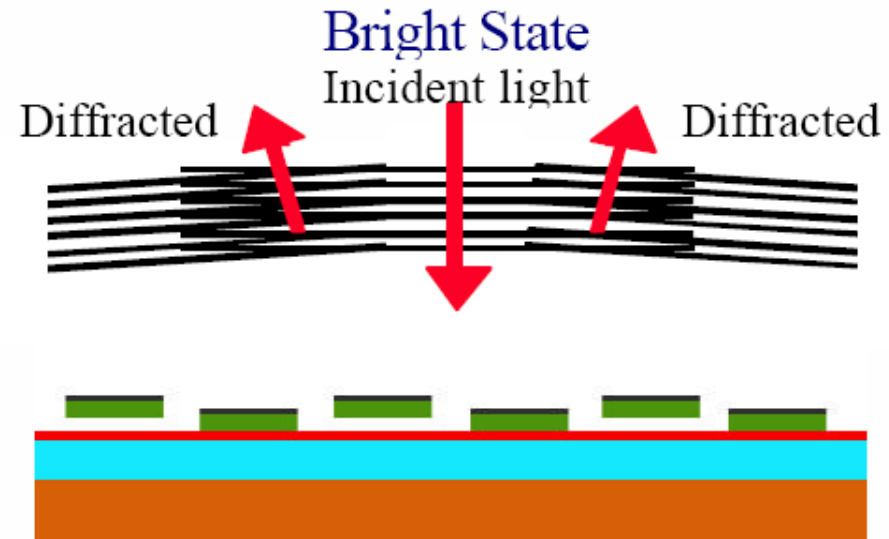
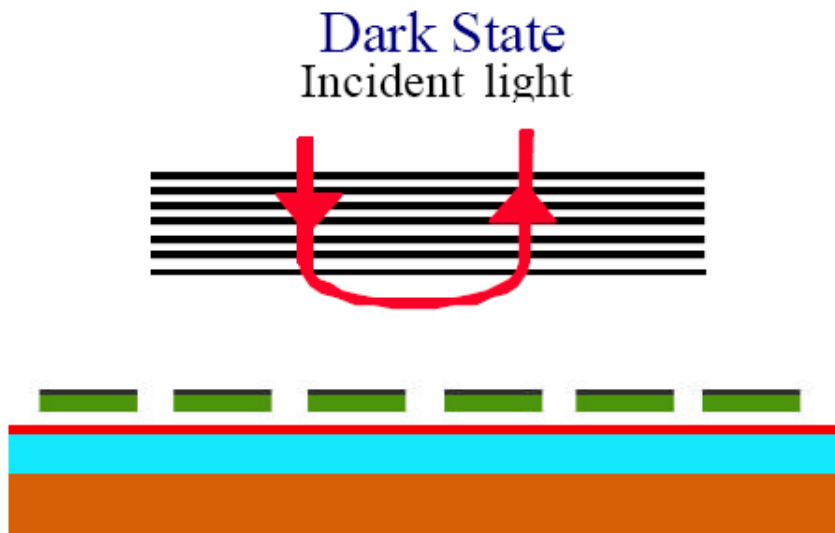
Diffraction

The grating light valve (GLV)

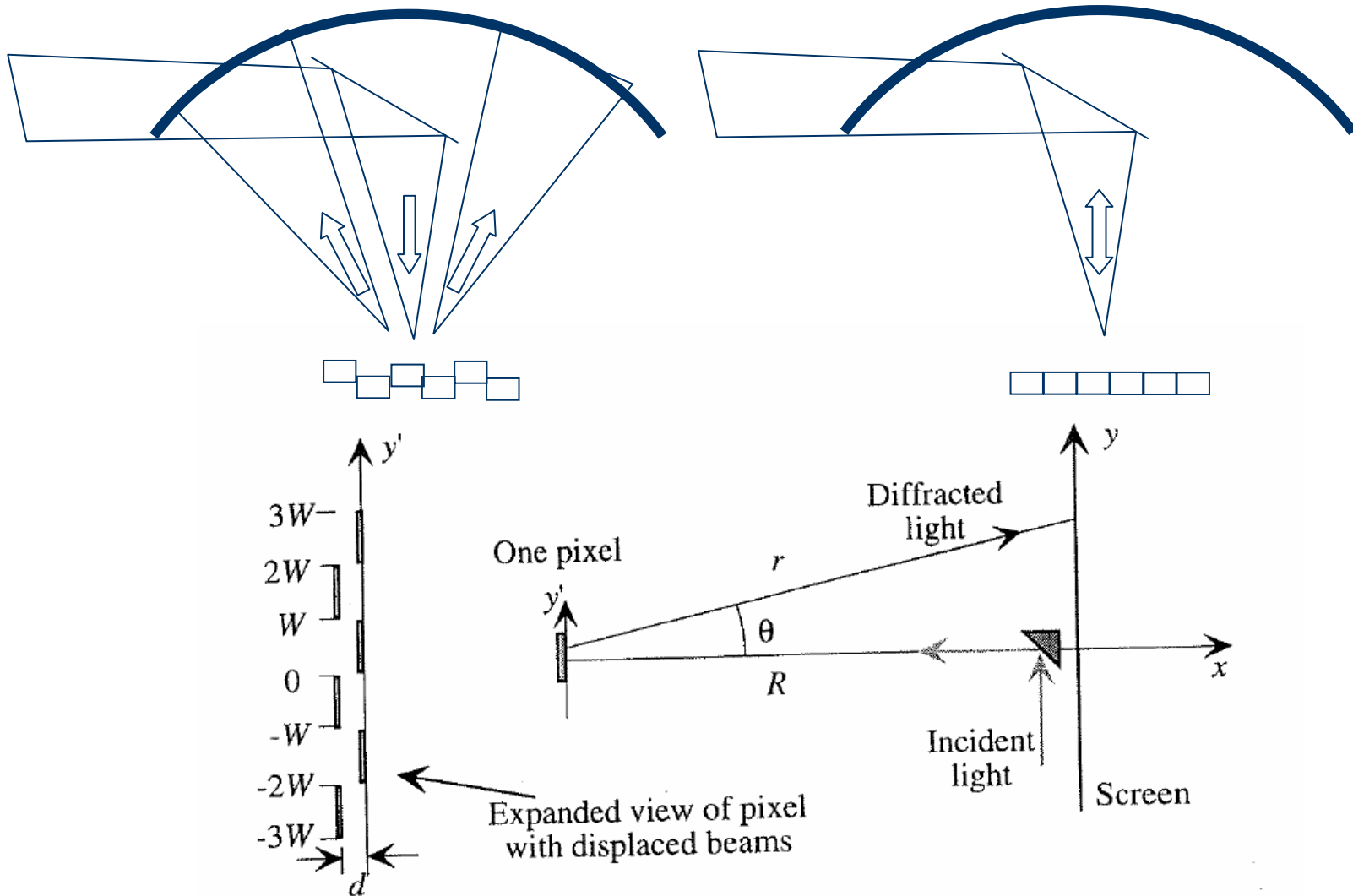
- Grating Light Valve
- Electrostatically deflect ribbons
- Distance to wafer $\lambda/4$
- Light is reflected or diffracted
- Diffracted light is projected to screen
- Possible to use pull-in or pull-control
- Possible to have one row of ribbon pixels only



Diffraction from a grating light valve



GLV used in a display device



Diffraction of Light

Maxwell's equations may be reduced to the scalar wave equation.

$$\begin{aligned}\nabla \times \vec{H} &= \epsilon \frac{\partial \vec{E}}{\partial t} \\ \nabla \times \vec{E} &= -\mu_0 \frac{\partial \vec{H}}{\partial t} \\ \nabla \cdot \vec{E} &= 0 \\ \nabla \cdot \vec{H} &= 0,\end{aligned} \quad \Longrightarrow \quad \nabla^2 U = \frac{n^2}{c^2} \frac{\partial^2 U}{\partial t^2}$$

U may be any component of vectors H and E

Assumptions: *Linear, isotropic*, homogeneous and non-dispersive

Diffraction of light

$$\nabla^2 U = \frac{1}{c^2} \frac{\partial^2 U}{\partial t^2}$$

Example solutions of the wave equation are the plane wave and spherical wave:

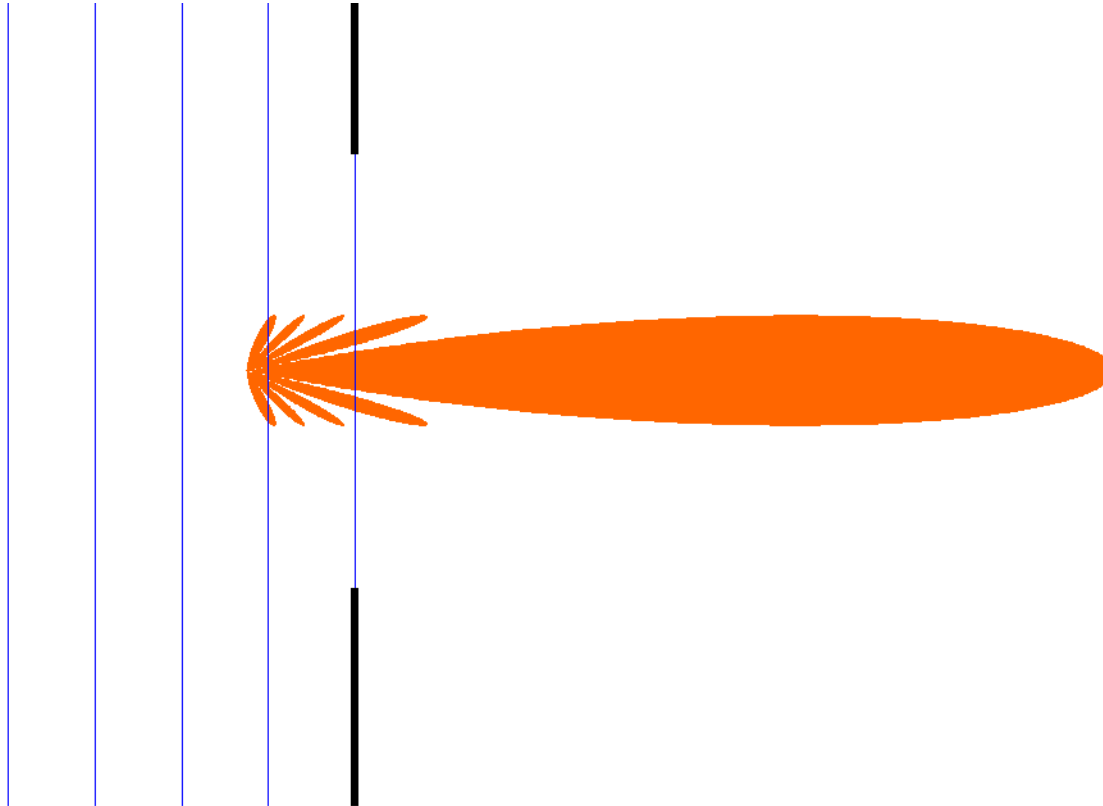
$$U = U_0 \exp(i\vec{k}\vec{r} - \omega t - \phi)$$

$$|\vec{k}| = k = \omega/c$$

$$U = \frac{U_0}{r} \exp(ikr - \omega t - \phi)$$

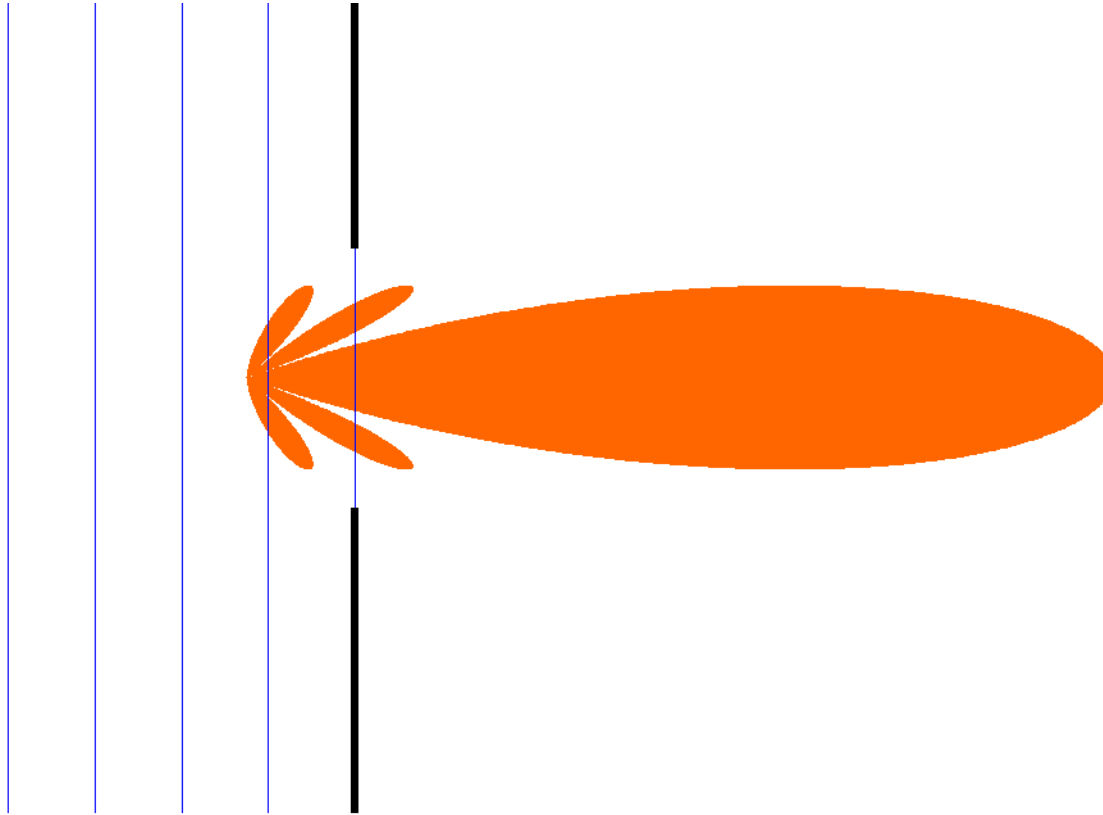
Diffraction of light

Light bends or diffracts around edges. Small apertures give large diffraction angles



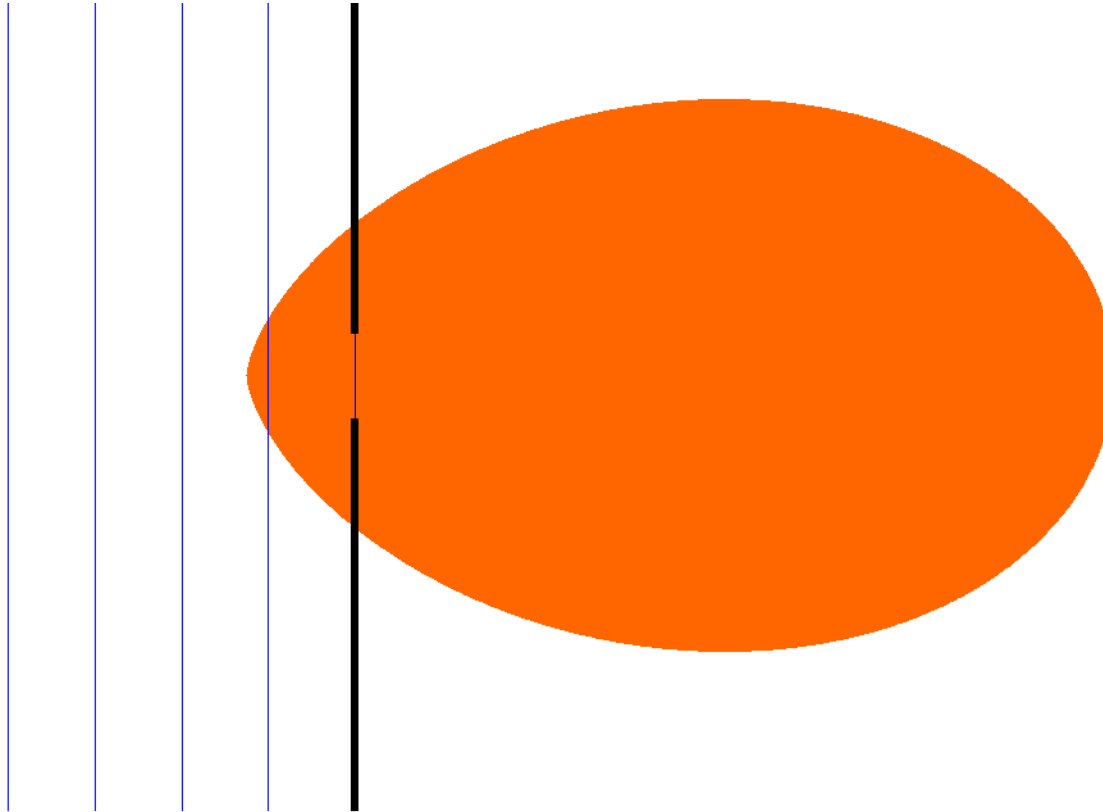
Diffraction of light

Light bends or diffracts around edges. Small apertures give large diffraction angles



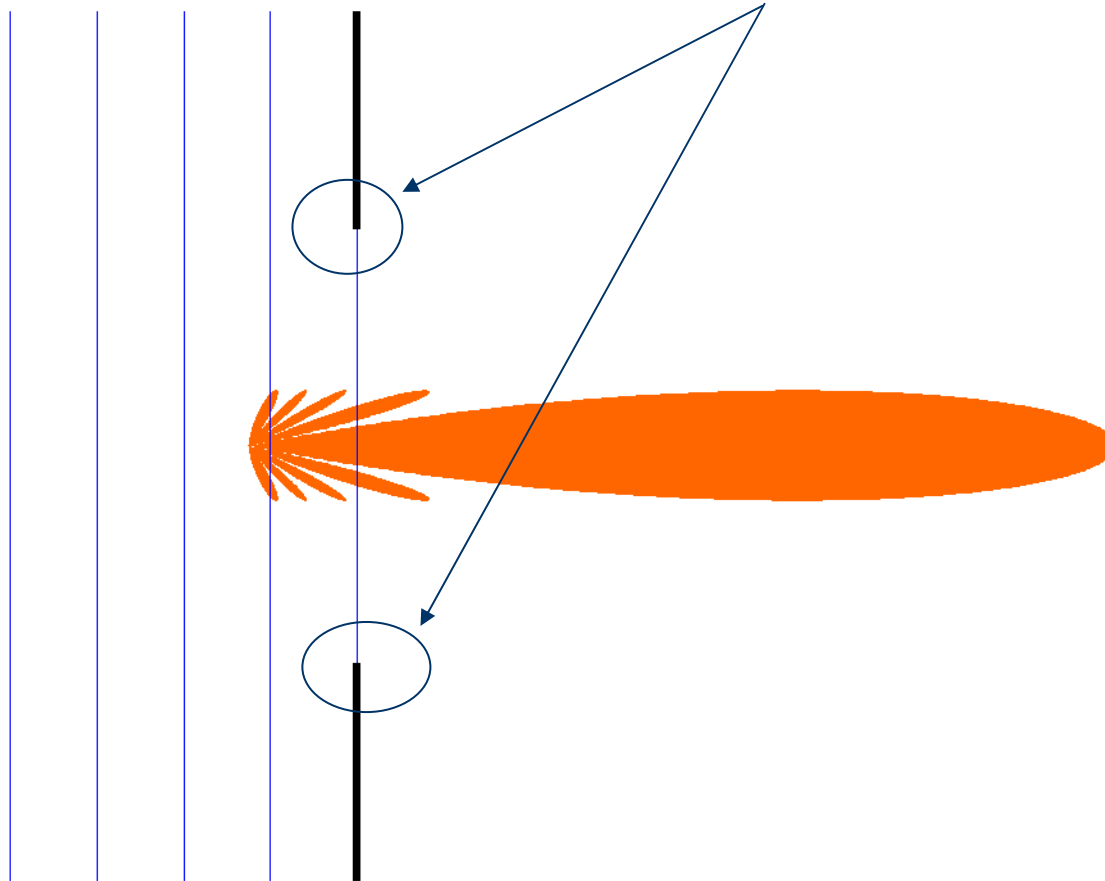
Diffraction of light

Light bends or diffracts around edges. Small apertures give large diffraction angles



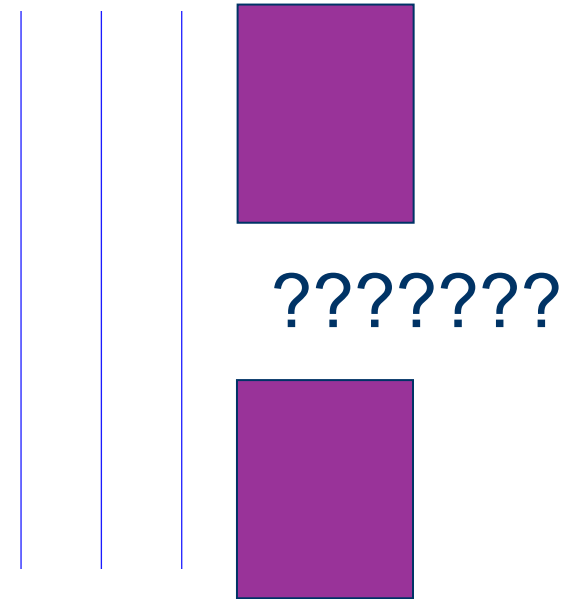
Diffraction of light

Here, edge effects are small



Diffraction of light

When edges are thick and holes are small, scalar diffraction theory is no longer valid



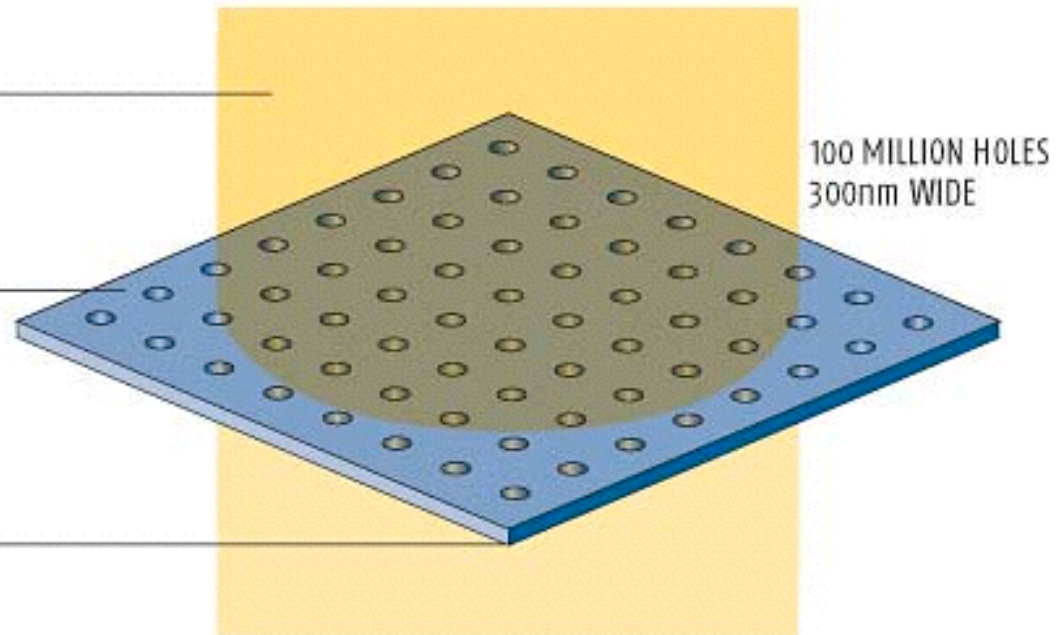
USING SURFACE PLASMONS TO CHANNEL LIGHT

Surface plasmons channel light towards the holes, so more is transmitted than expected

Light falls onto a thin metal film and excites surface plasmons on the metal foil

The surface plasmons accumulate so much energy around the holes that the resulting electric field penetrates the metal

Surface plasmons on the underside of the metal foil convert the energy back into light

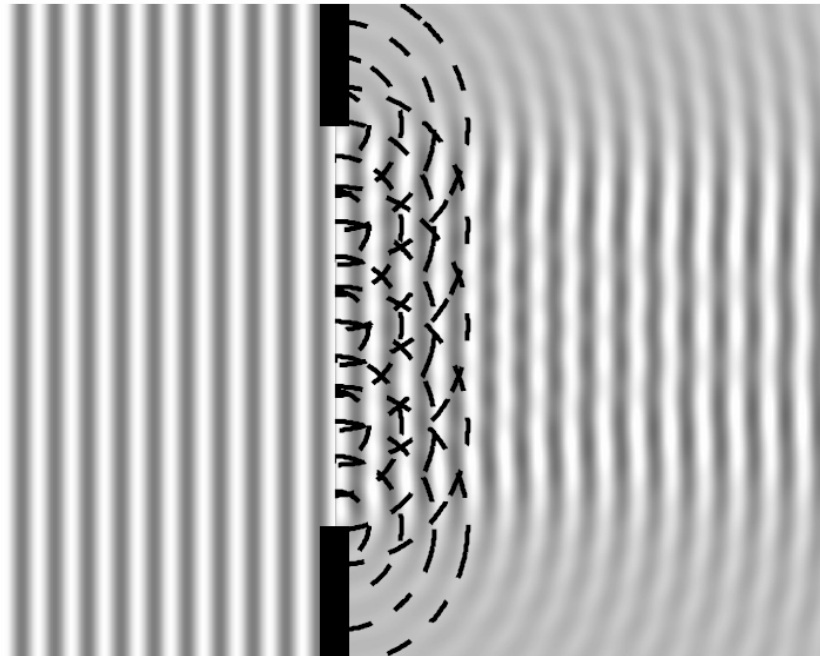


The *Huygens-Fresnel principle* says:

”The light disturbance at a point P arises from the superposition of secondary waves that proceed from a surface situated between this point and the light source.”



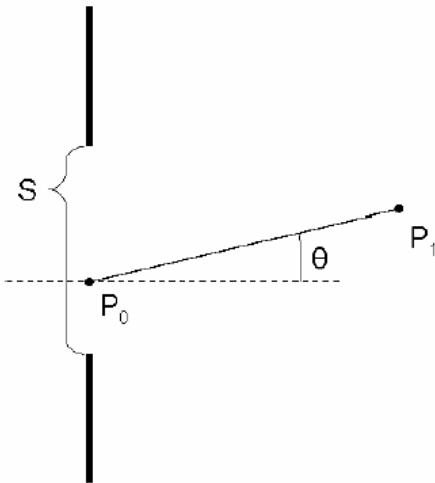
Christiaan Huygens



Augustin-Jean
Fresnel

Diffraction of Light

A mathematical representation of the Huygens-Fresnel principle:



$$U(P_1) = \frac{1}{i\lambda} \iint_S U(P_0) \frac{\exp(ikr_{01})}{r_{01}} \cos \theta ds$$



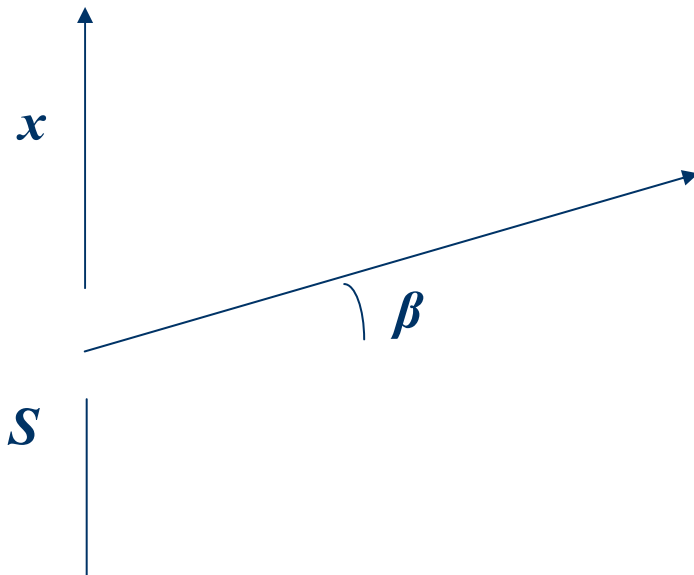
Spherical wave

Diffraction of Light

Far away from the aperture, and for small diffraction angles we may use the Fraunhofer approximation.



$$U(\beta) = C \int_S U(x) \exp(ik\beta x) dx$$

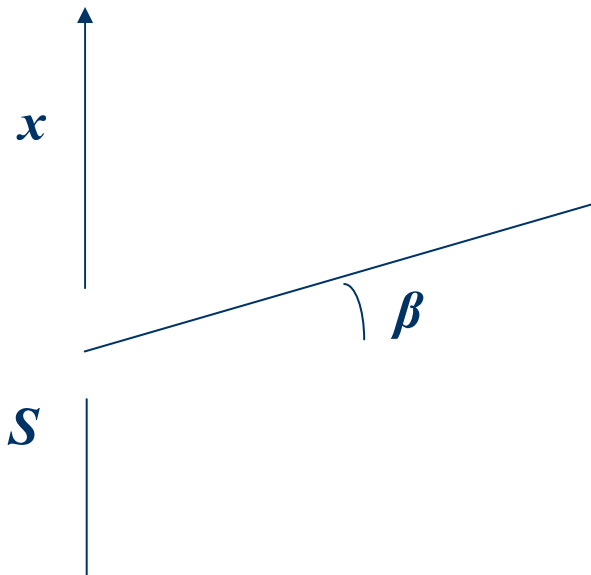


Diffraction of Light

Far away from the aperture, and for small diffraction angles we may use the Fraunhofer approximation.



$$U(\beta) = C \int_S U(x) \exp(ik\beta x) dx$$



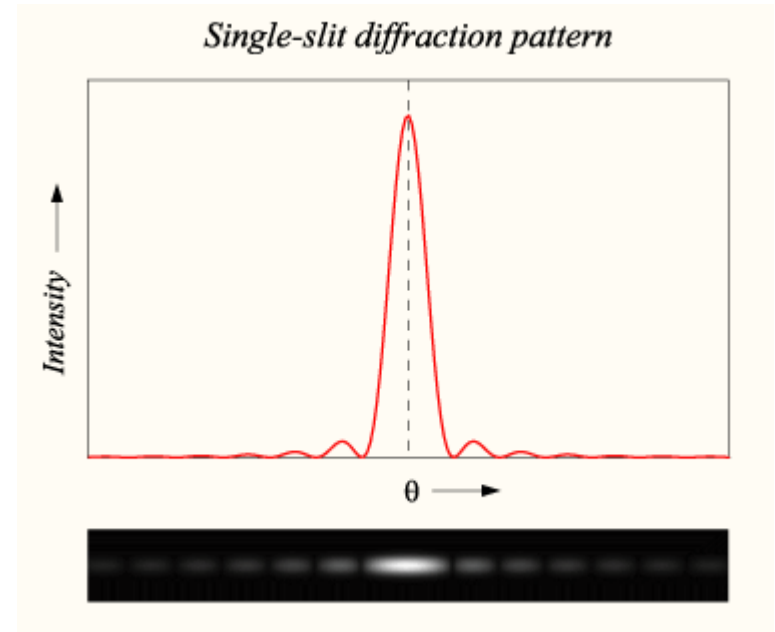
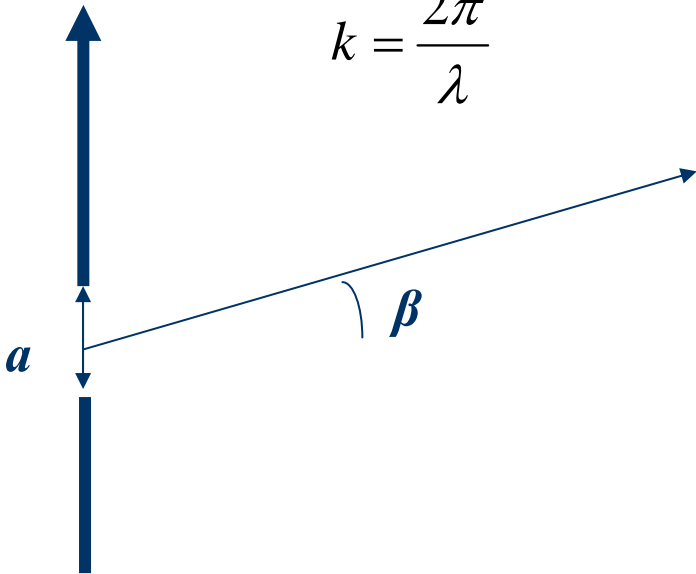
Fourier transform!

Diffraction of Light

We may now calculate the diffraction from a slit:

$$I = \left[\frac{\sin\left(\frac{k\beta a}{2}\right)}{\left(\frac{k\beta a}{2}\right)} \right]^2$$

$$k = \frac{2\pi}{\lambda}$$

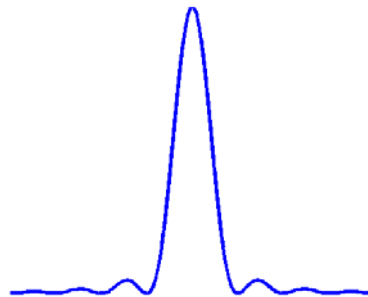
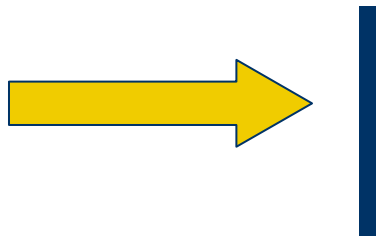
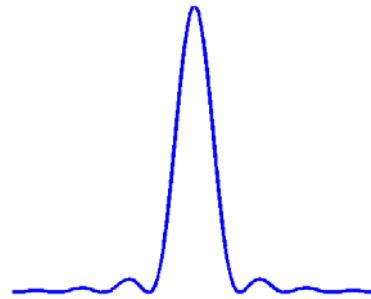
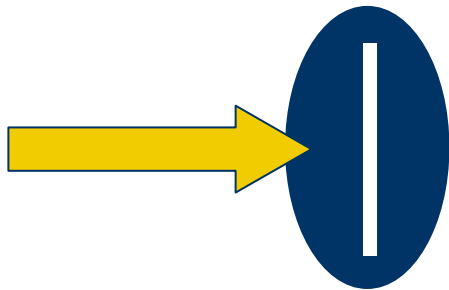


Minima for:

$$\beta = m \frac{\lambda}{a}$$

Babinet's principle

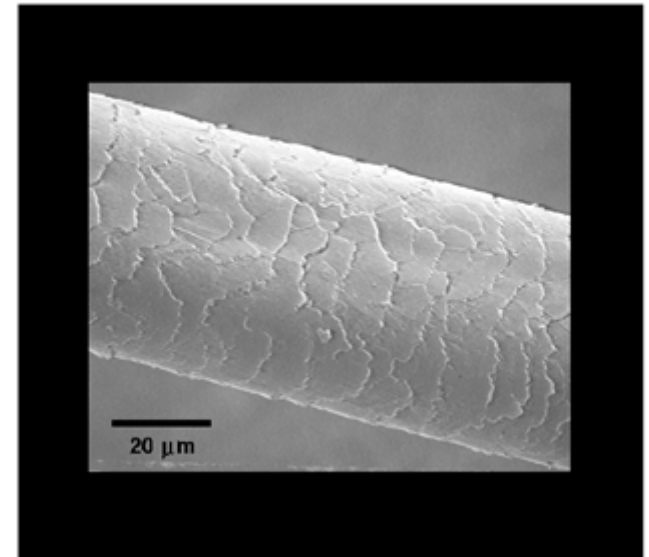
The diffracted field from an aperture is the same as from an obscuration of the same size and shape



Collection Ecole polytechnique



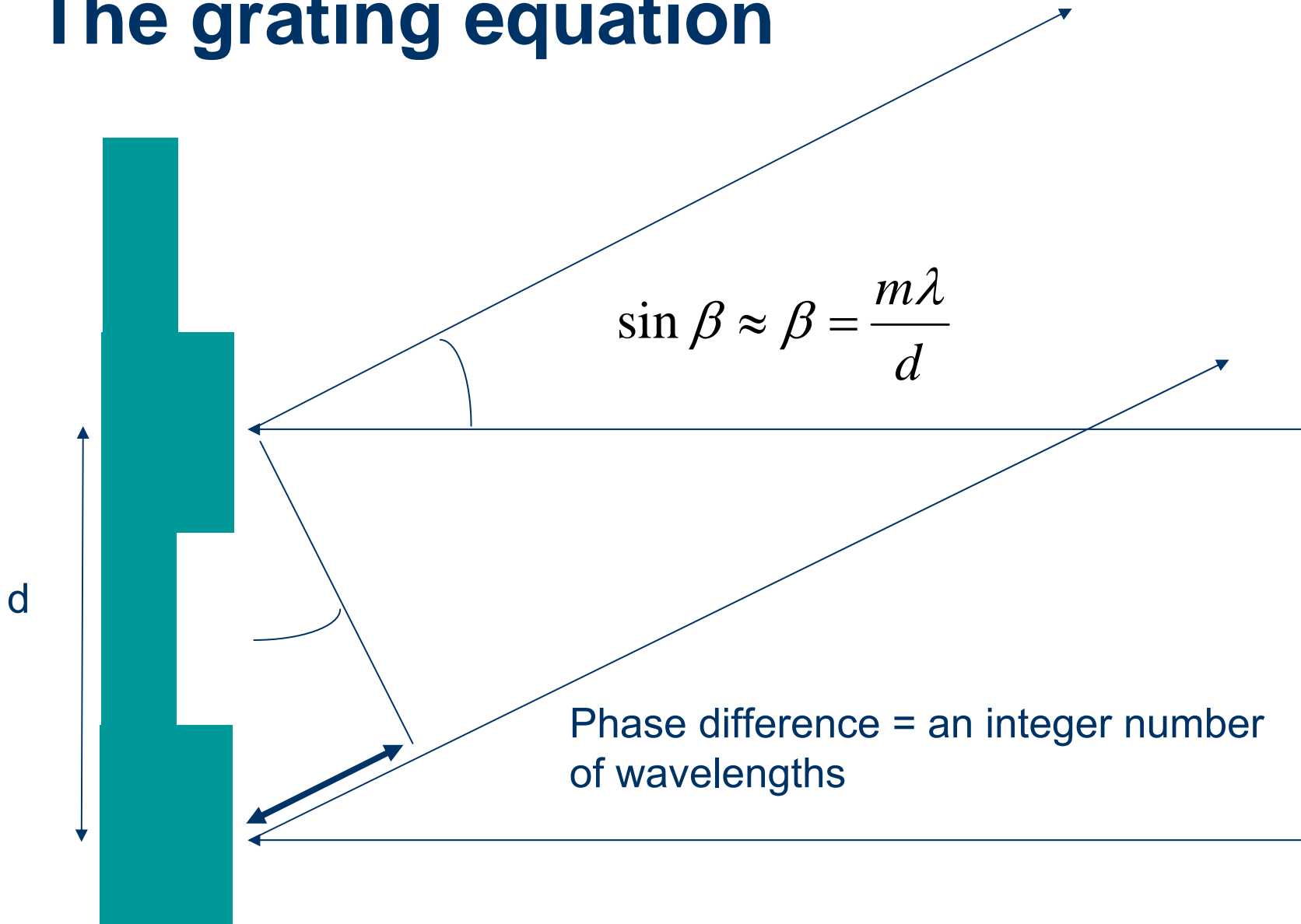
Jacques Babinet (1794-1872) X 1812



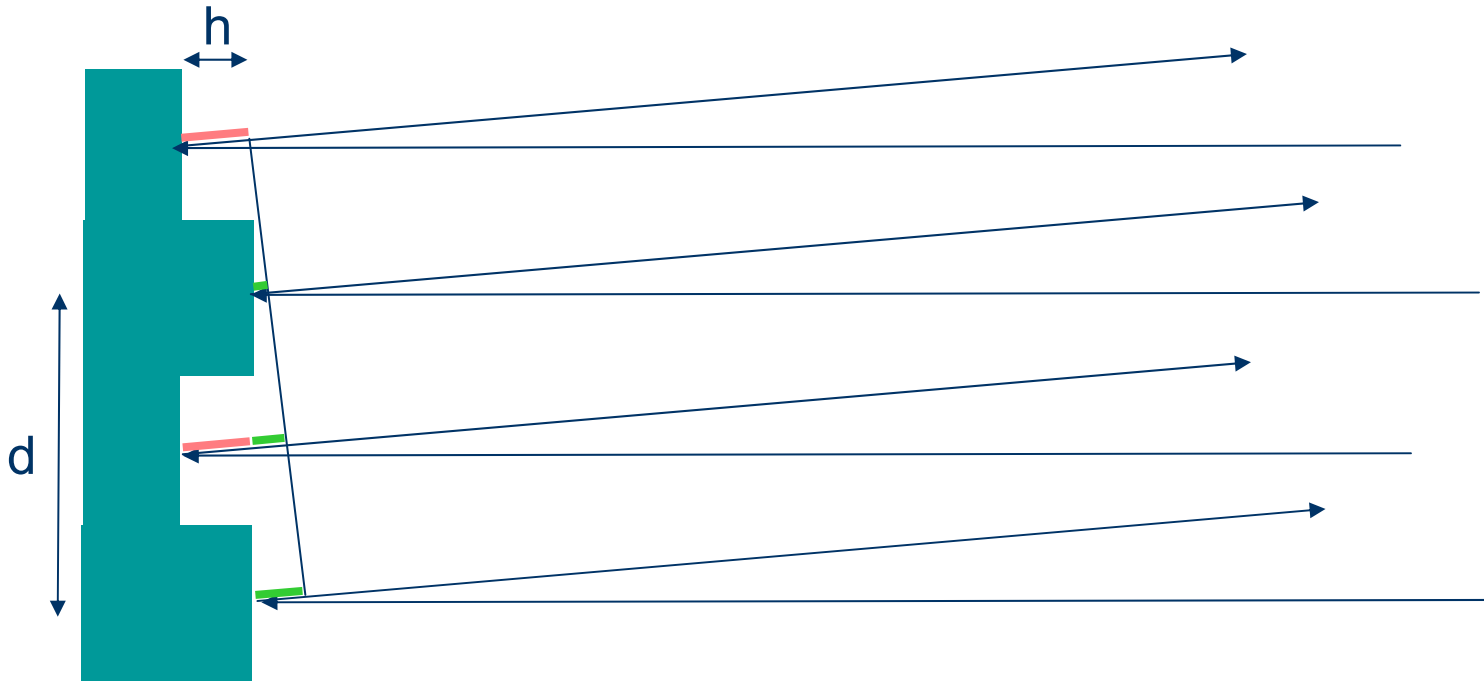
Diffraction from a grating light valve



The grating equation

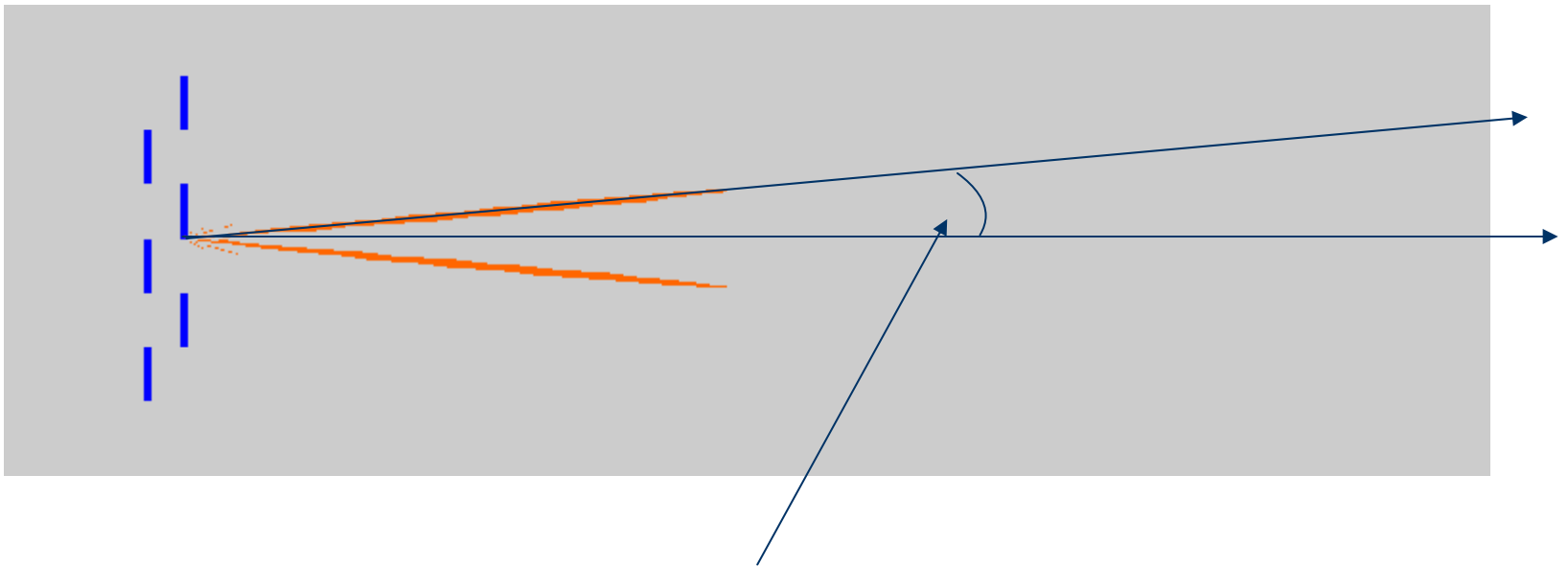


Diffraction from a grating light valve



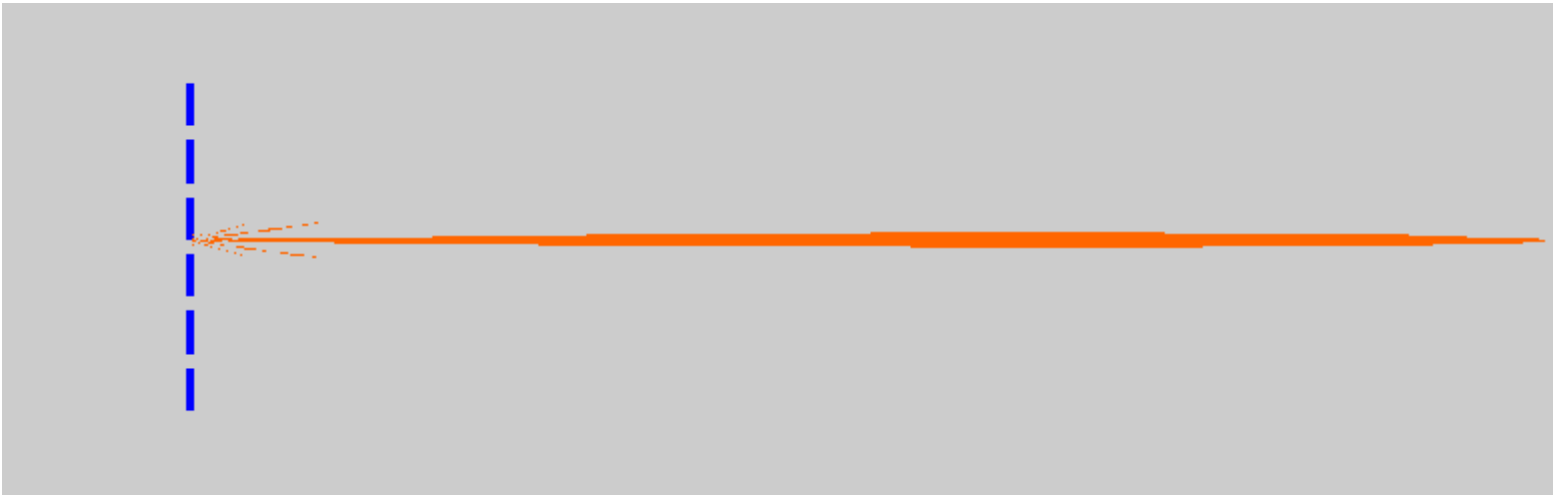
$$\frac{I}{I_0} = \left| \frac{U}{U_0} \right|^2 = \frac{4}{\pi^2} \sin^2(kh)$$

Diffraction from a grating light valve



Angle given by the grating equation

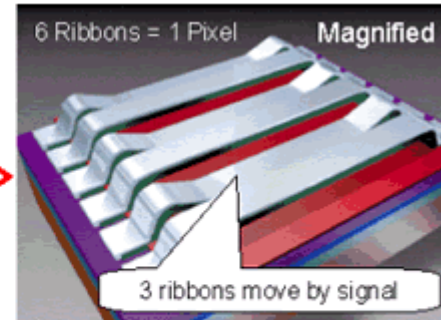
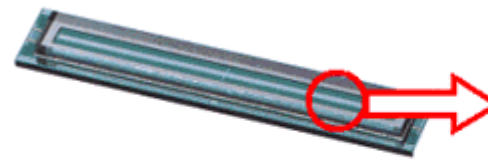
Diffraction from a grating light valve



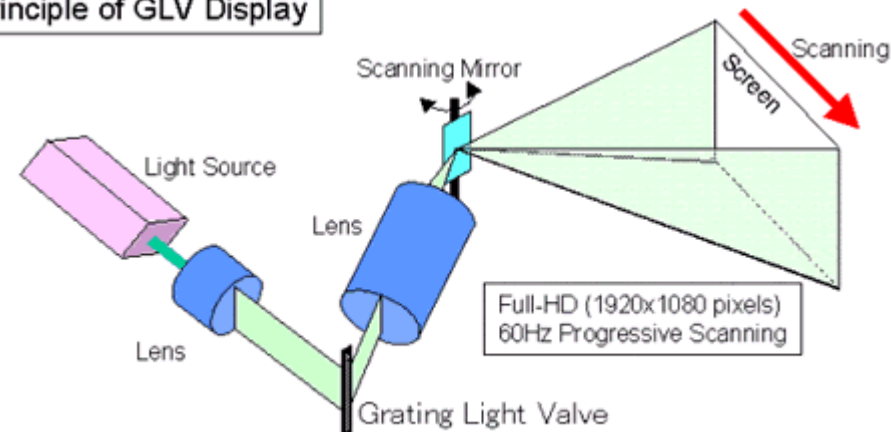
How to design a GLV display device



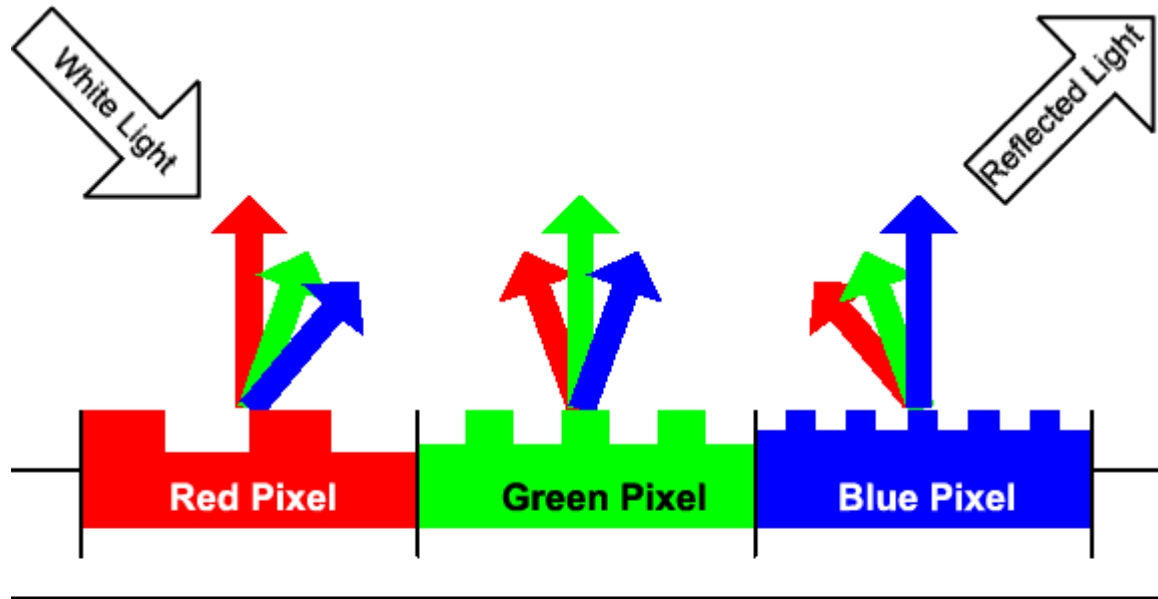
Structure



Principle of GLV Display



Different pixels for different wavelengths



With all ribbons in a pixel in the rest position, light striking the pixel is reflected away from the optical path. When alternate ribbons are pulled down, the diffraction grating is formed and the light's component frequencies spread out. Varying the width and spacing of the ribbons "tunes" pixels to send a single colour into the projector's light path.

How to design a GLV display device

One line of mirror elements only

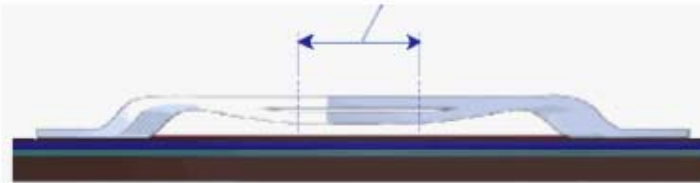
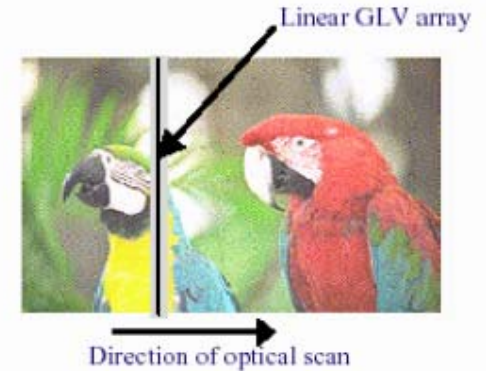
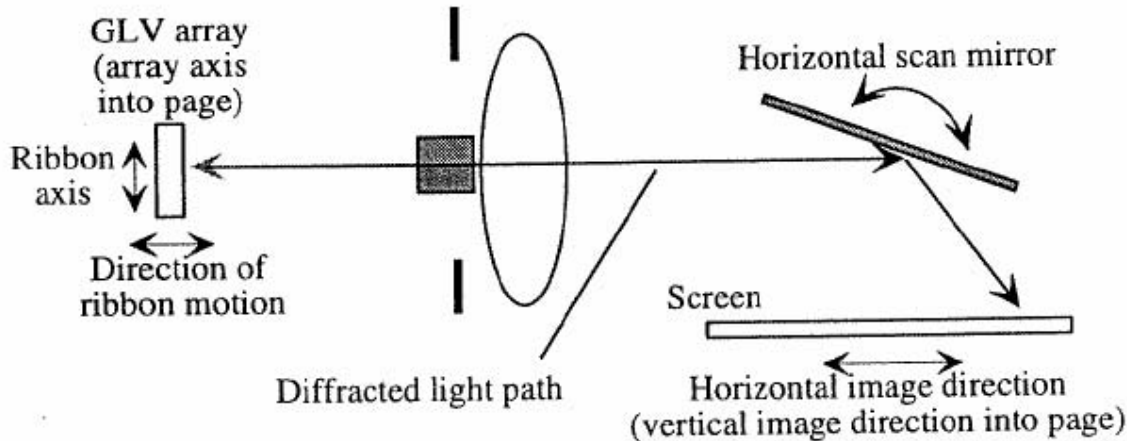
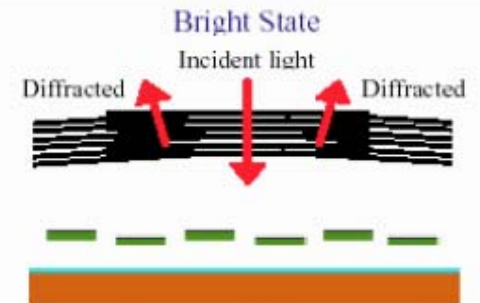


Figure 1: A GLV pixel with alternate reflecting ribbons electrostatically deflected to produce a square-well diffraction grating (vertical deflection greatly exaggerated)



Grating light valves

- Can you spot the difference between the top and bottom GLV?

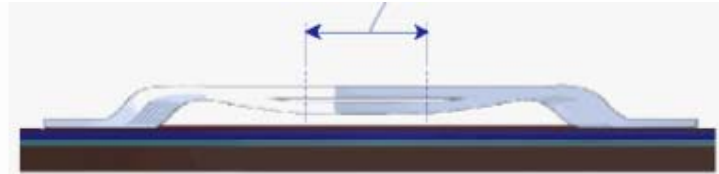
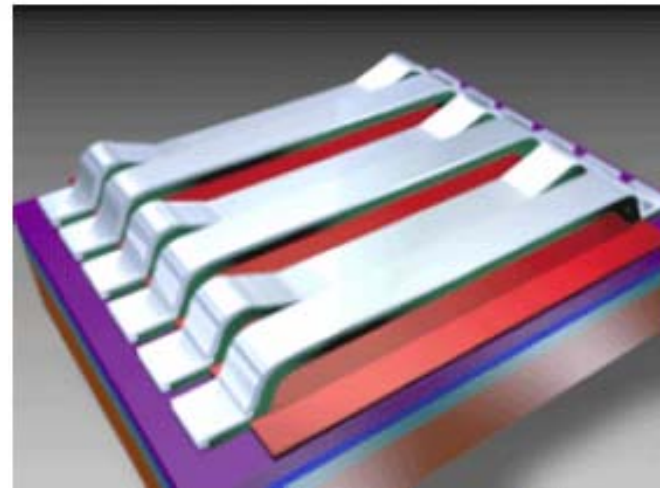
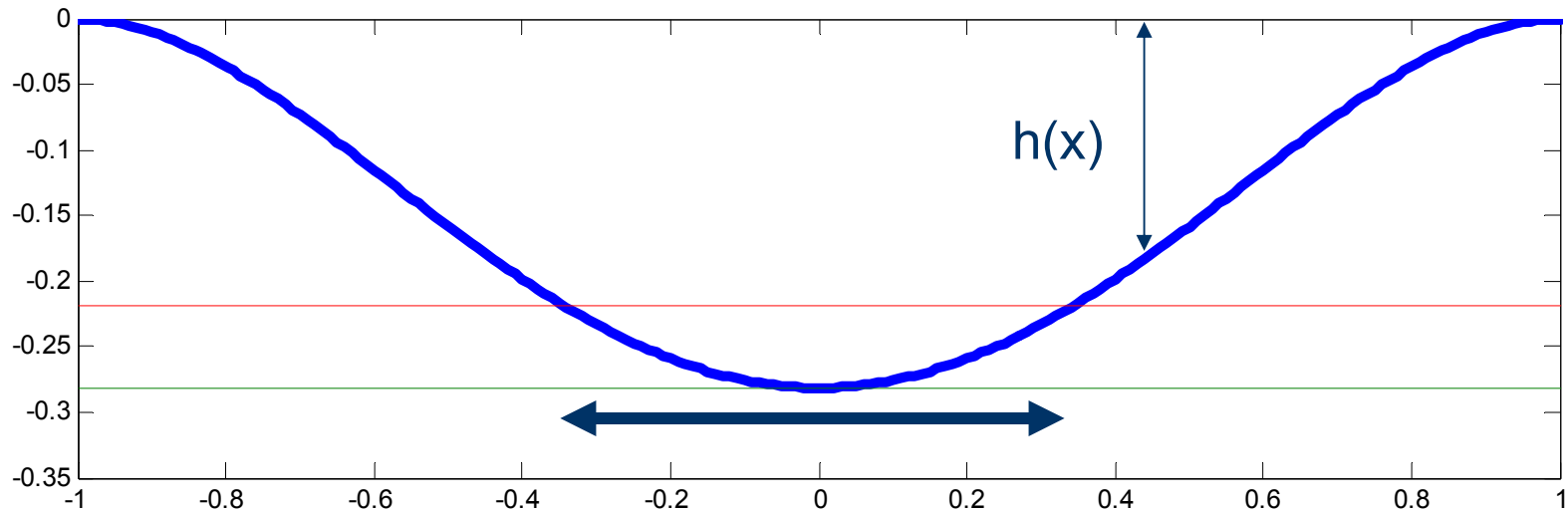


Figure 1: A GLV pixel with alternate reflecting ribbons electrostatically deflected to produce a square-well diffraction grating (vertical deflection greatly exaggerated)



The clamped-clamped beam with distributed load



Must integrate
diffraction efficiency
over the length of
the beam:

$$\frac{I}{I_0} = \frac{4}{\pi^2 L} \int \sin^2 [kh(x)] dx$$

How to design a GLV display device:

Challenges

- High optical throughput requires large diffraction angle and short grating periods
- The shorter the period the more light is lost in the gaps between the ribbons
- Clamped-clamped beams/ribbons result in low fill factor
 - Only a fraction of the beam is optically useful
- Different wavelengths require different modulation heights

"Grating light valves" for spectroscopy

- "Polychromator"
- SINTEF CDOE

Polychromix/Senturia

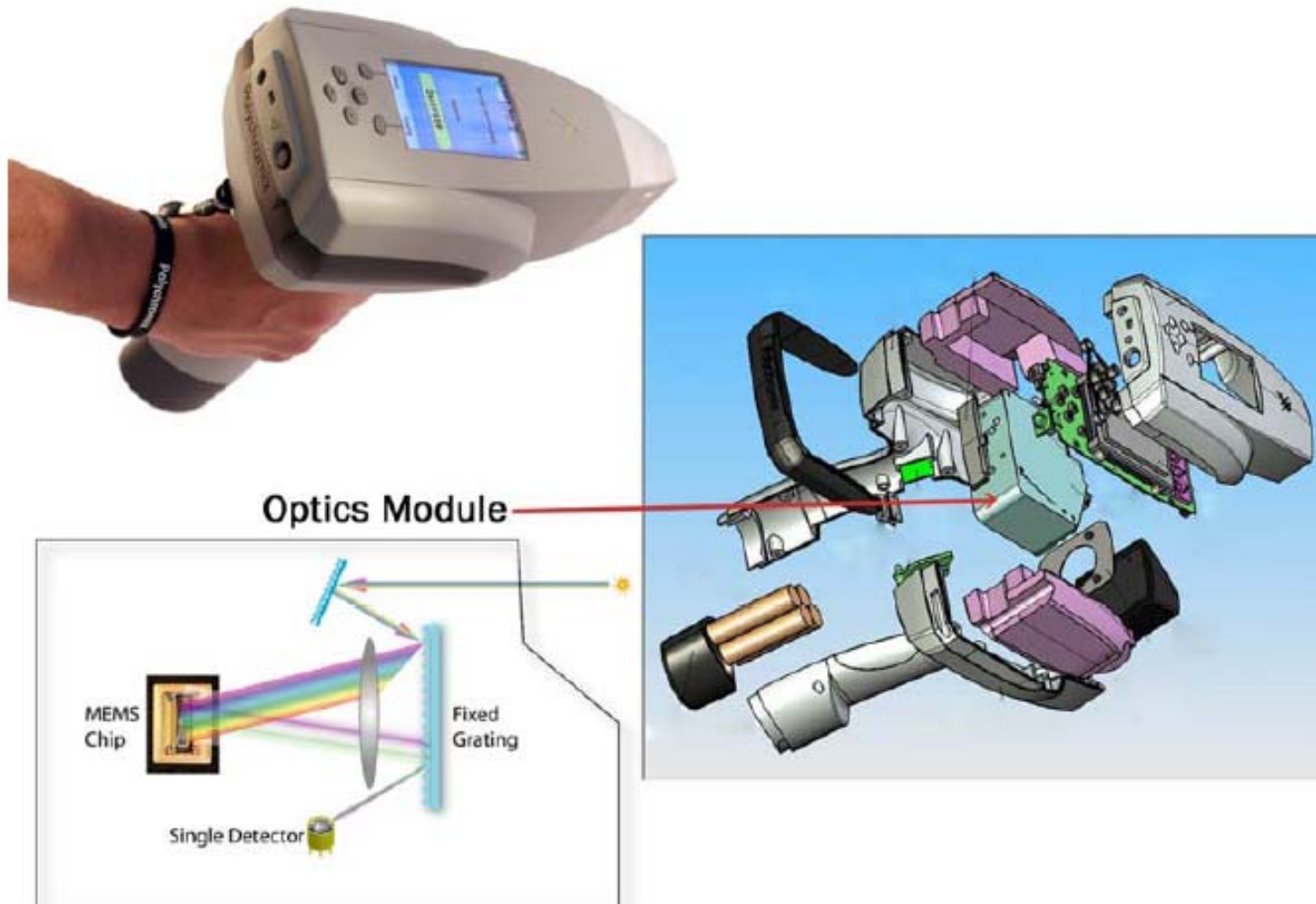


Figure 2: The PHAZIR™ along with an exploded view revealing the optics module with the MEMS chip inside. The optical architecture is shown in the inset.

Polychromix (Senturia)

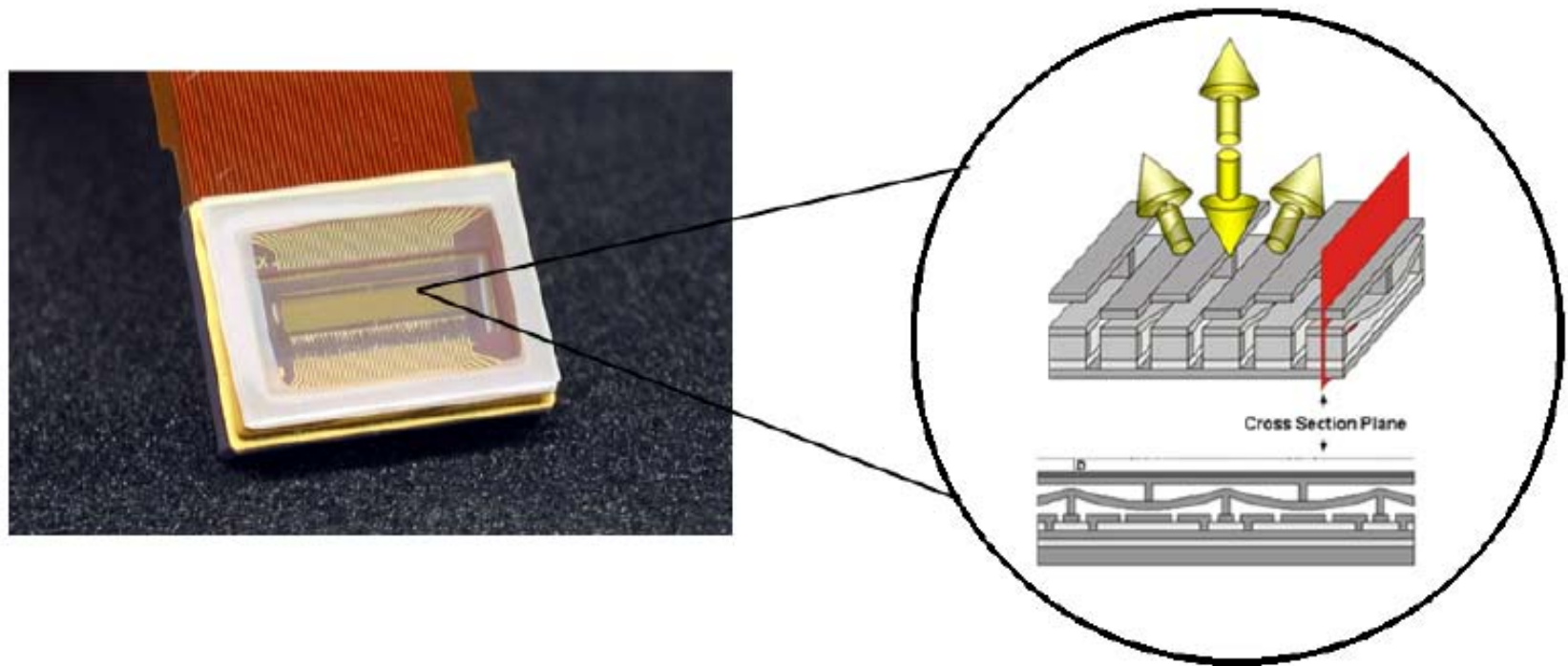
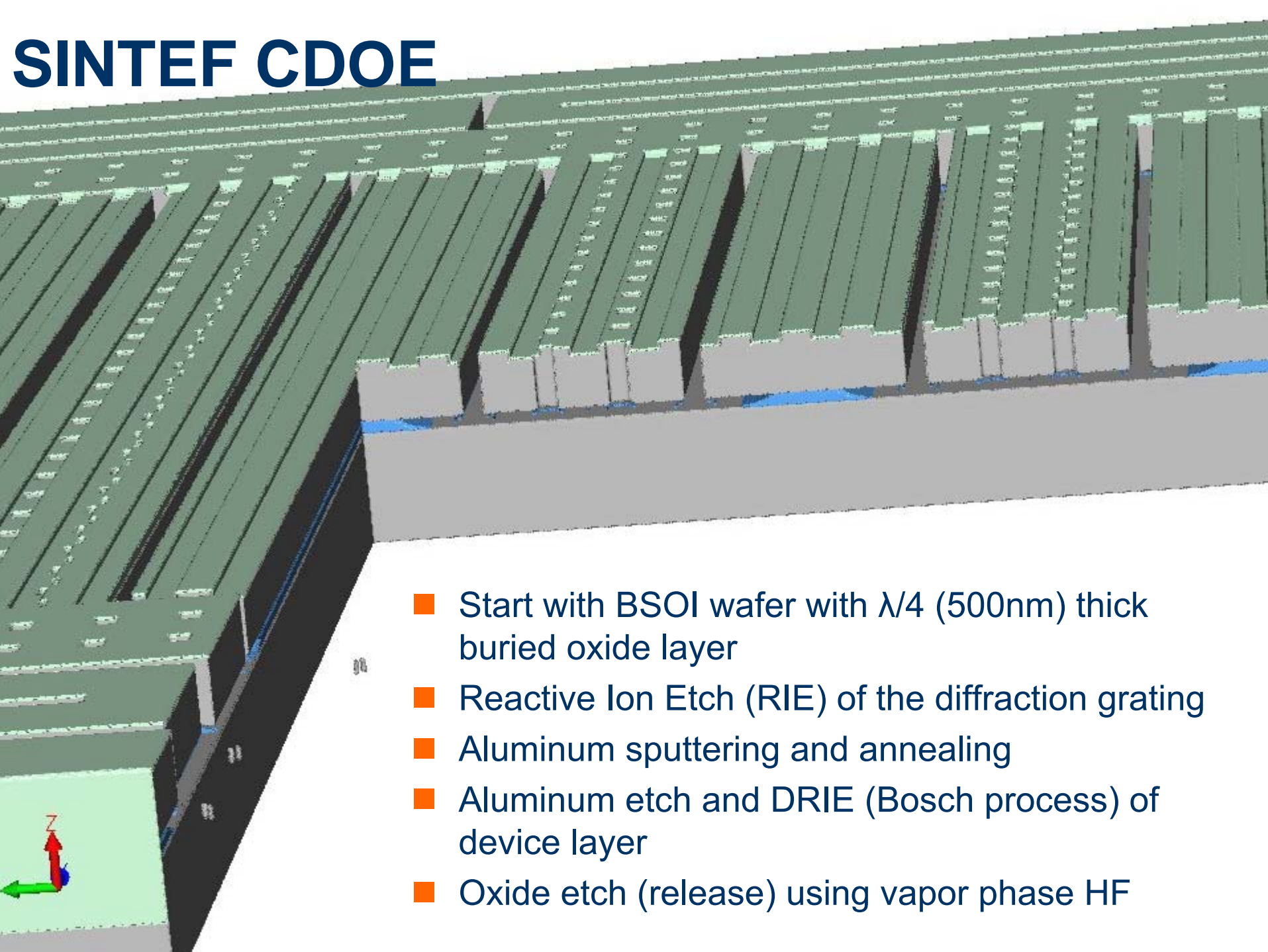


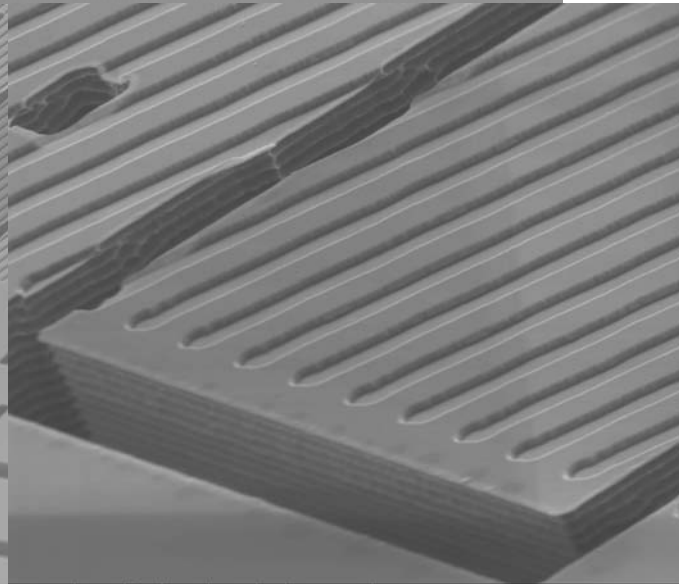
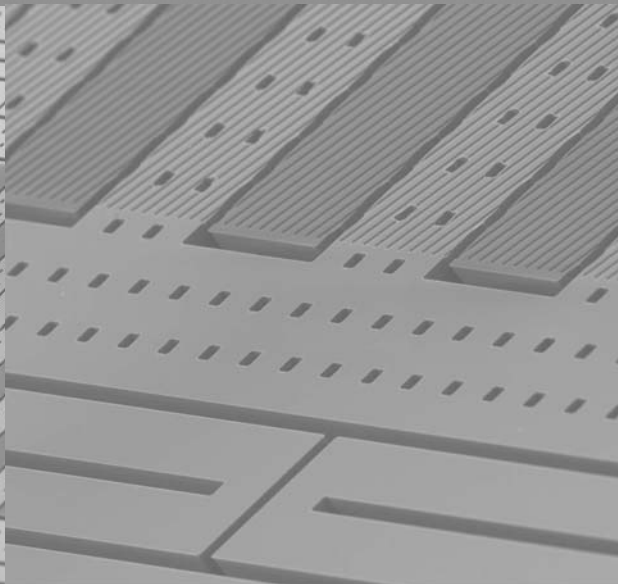
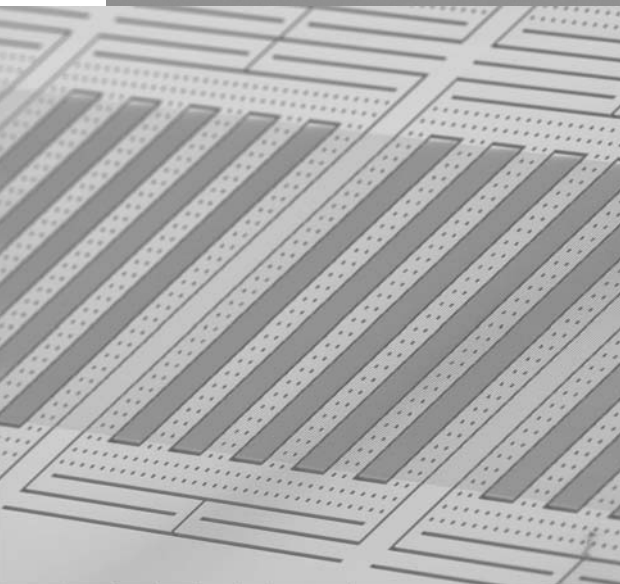
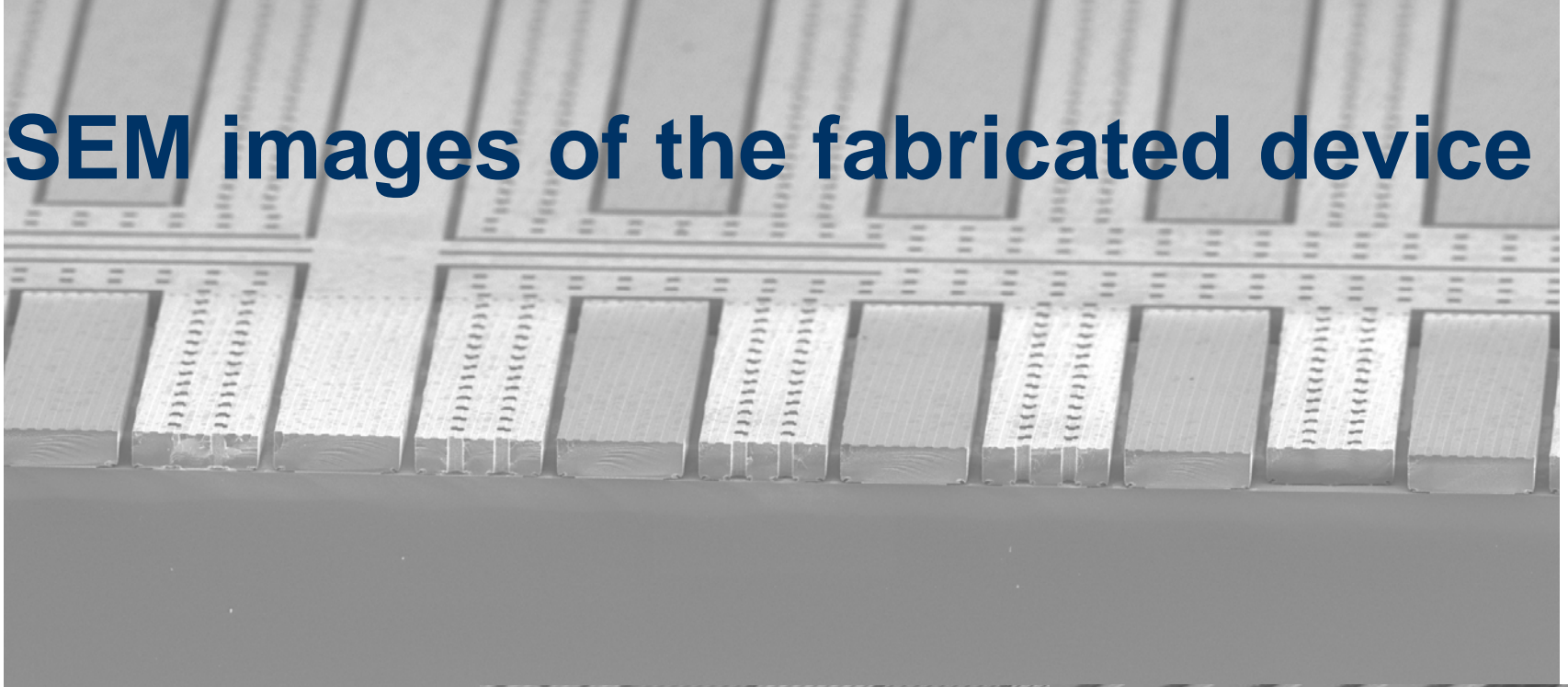
Figure 1: A packaged MEMS chip with a schematic illustration of its operation as an electrically programmable diffraction grating.

SINTEF CDOE



- Start with BSOI wafer with $\lambda/4$ (500nm) thick buried oxide layer
- Reactive Ion Etch (RIE) of the diffraction grating
- Aluminum sputtering and annealing
- Aluminum etch and DRIE (Bosch process) of device layer
- Oxide etch (release) using vapor phase HF

SEM images of the fabricated device



WD 9.78 mm HV 5.0 kV Spot 4.0 Tilt 29.6 ° Mag 418x Det X: 1.34 mm Etd Y: 2.32 mm

—100 μm—

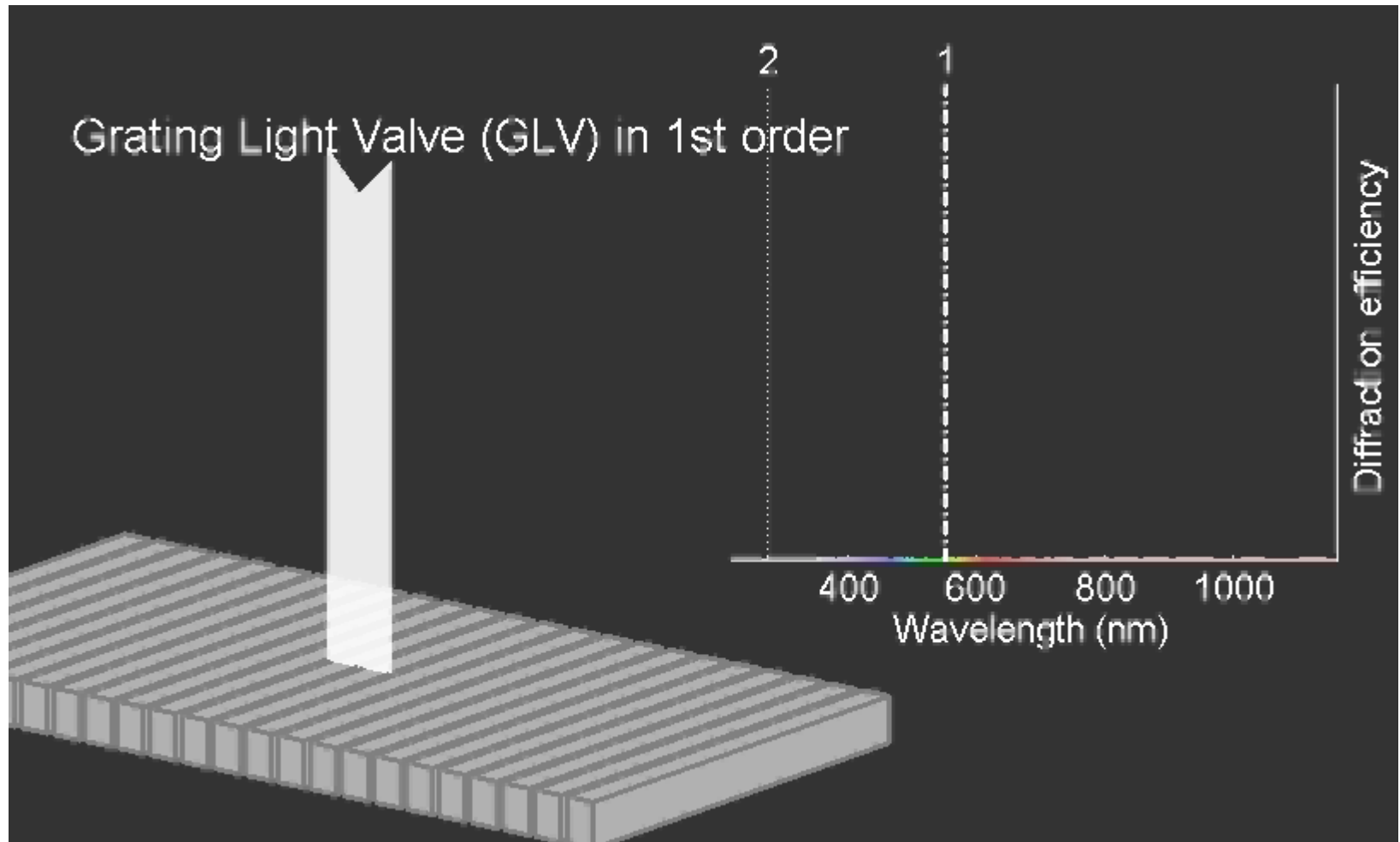
WD 10.01 mm HV 5.0 kV Spot 4.0 Tilt 29.6 ° Mag 1637x Det X: 1.23 mm Etd Y: 2.13 mm

—20 μm—

WD 9.85 mm HV 5.0 kV Spot 4.0 Tilt 29.7 ° Mag 8300x Det X: 1.33 mm Etd Y: 2.21 mm

—5 μm—

- This animation shows the principle of a first-order grating light valve. Only a narrow exit angle is considered.



Our aim is to measure *gas concentration* using a *micromechanical infrared filter*

The figure shows an old, established infrared sensing method for measuring gas concentration

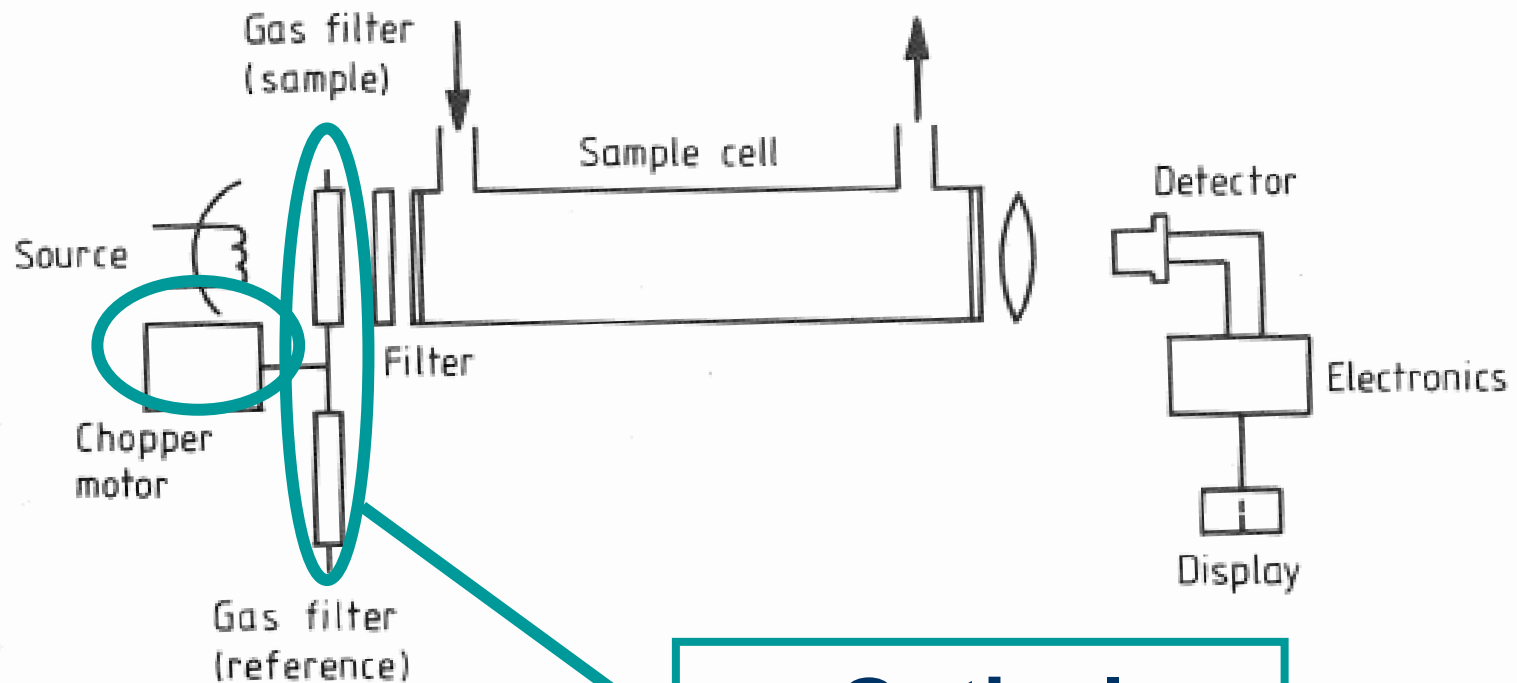
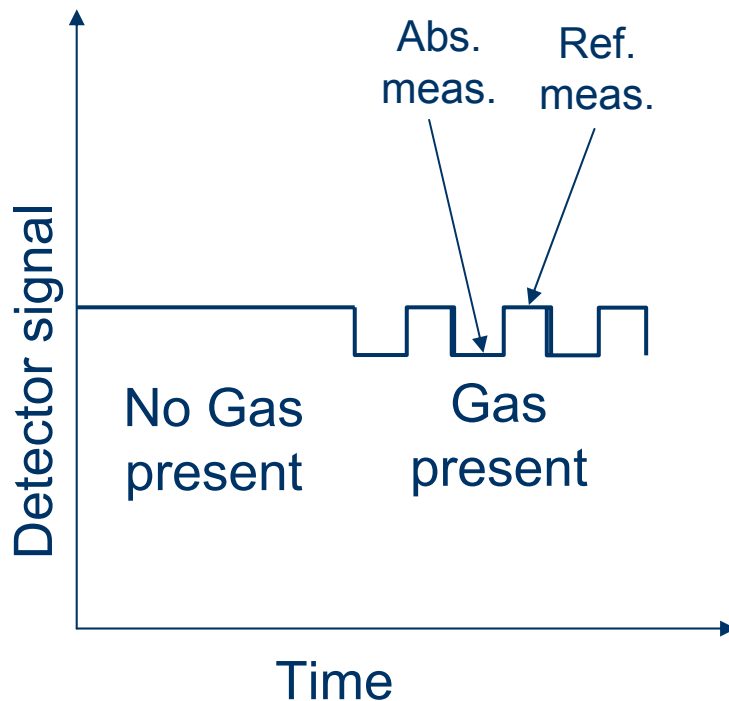


Image taken from Moseley et al,
"Techniques and mechanisms
in gas sensing"

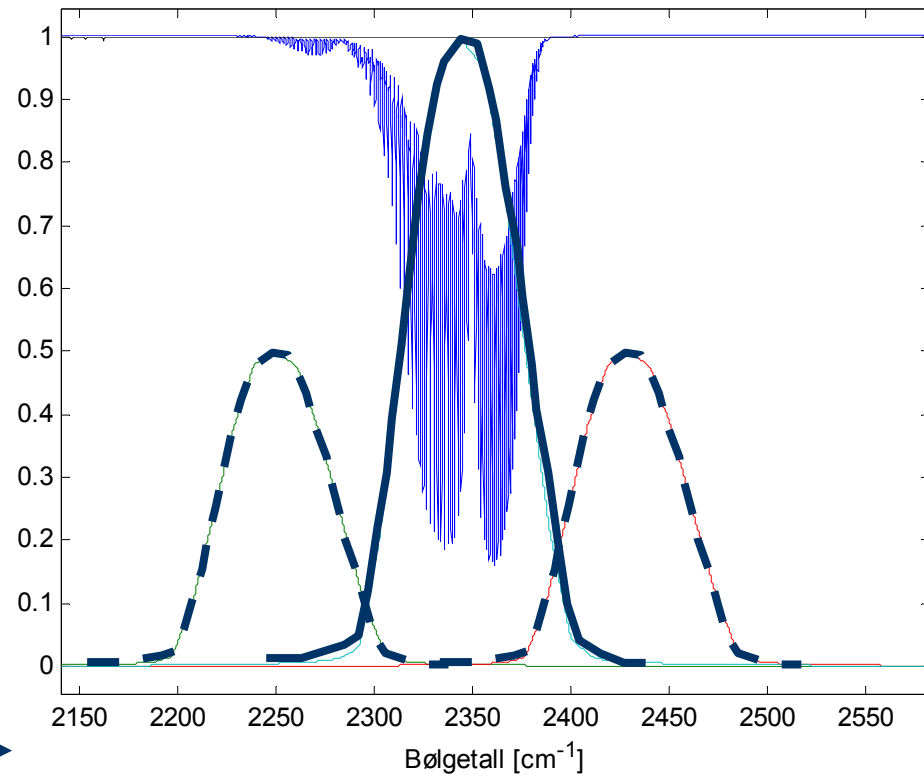
**Optical
MEMS device**

Reference measurements must be made in one or more wavelength bands outside the absorbing region

- Example: Carbon dioxide absorption
- Single detector
- Alternating filter

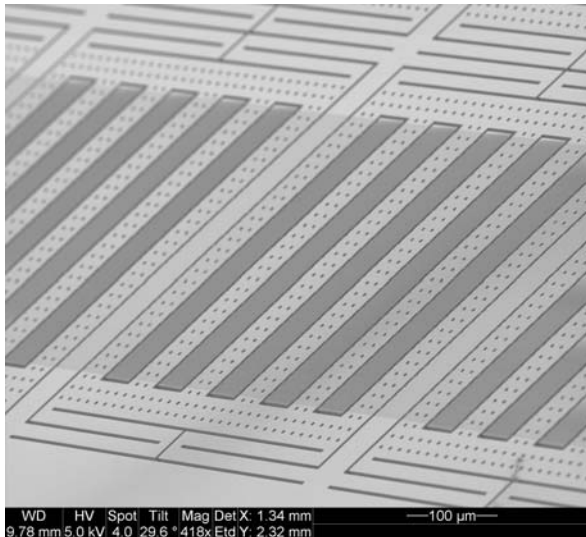
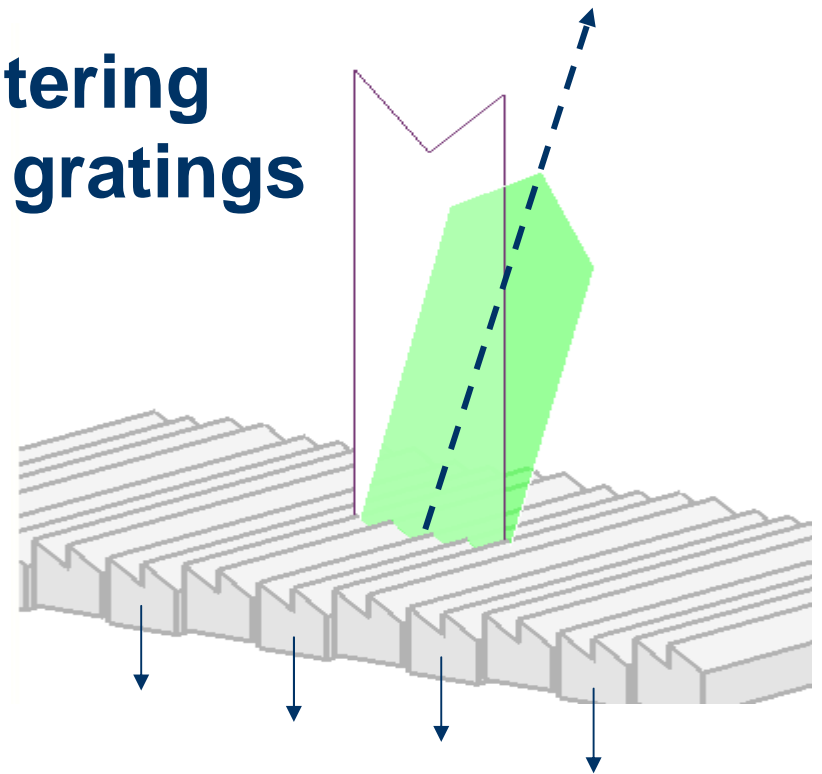


Infrared transmittance spectrum of CO₂



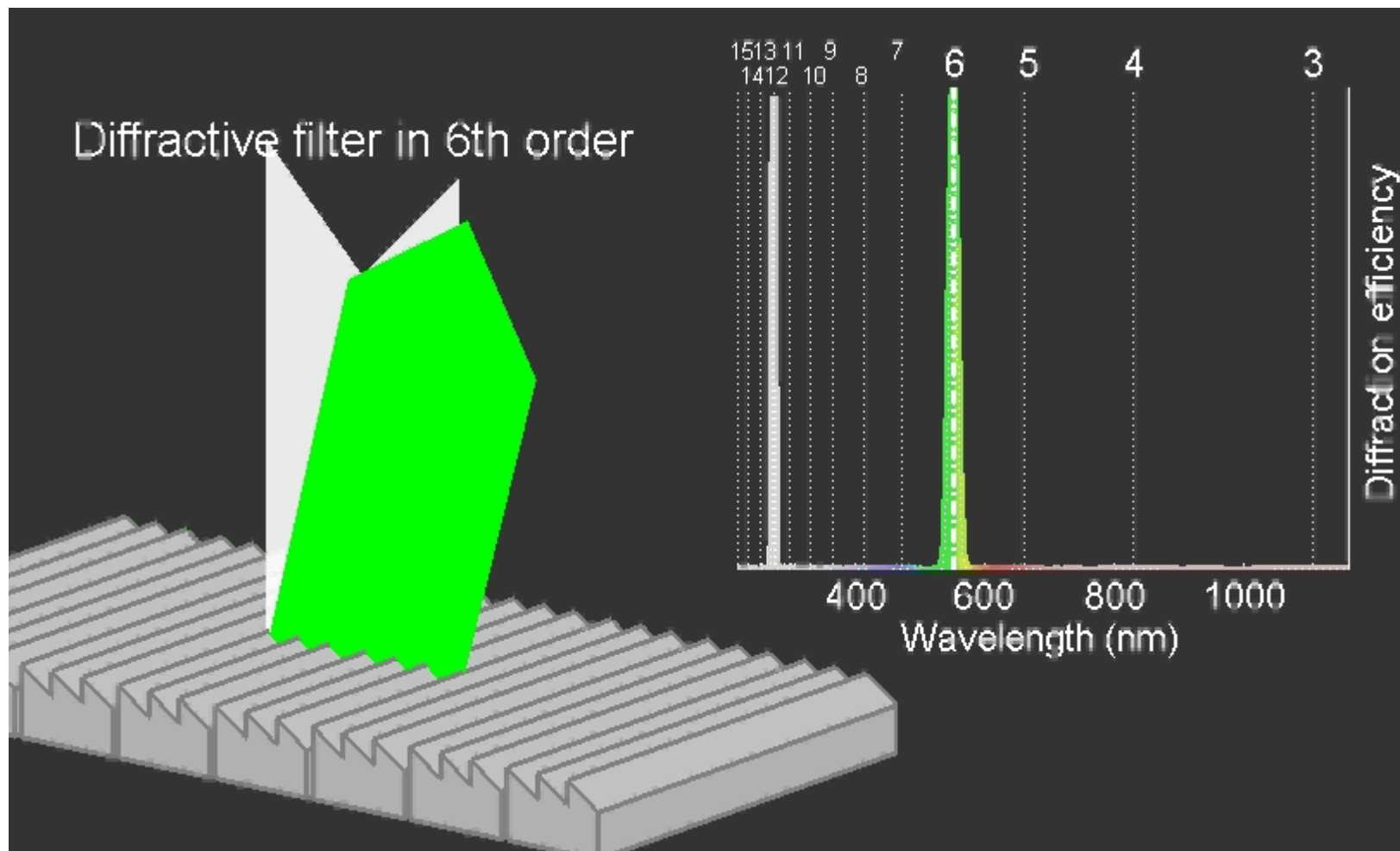
Design concept: Optical filtering with Modulated diffraction gratings

- Shine white light (broadband IR) onto a diffraction grating
- Collect the light diffracted into a chosen angle
- Change the color and intensity of the light by electromechanical modifications of the grating shape

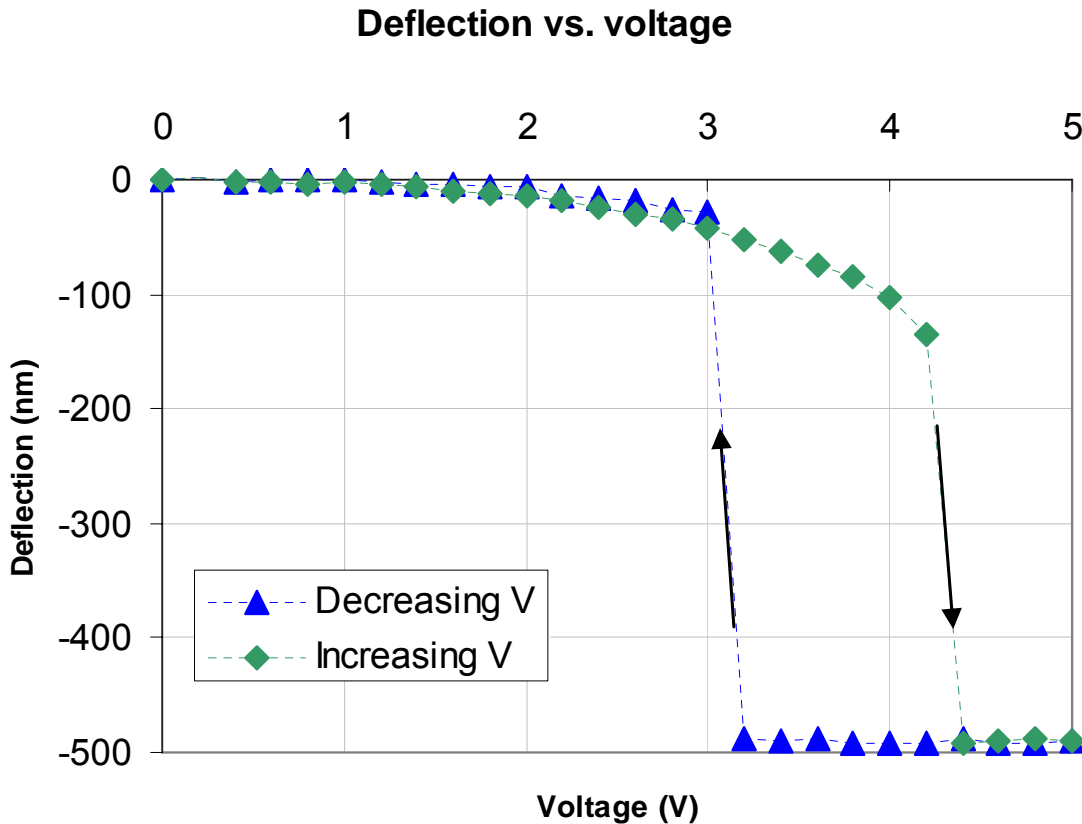


- Design objective:
 - Electromechanically simple
 - No position feedback
 - No calibration
 - No drift
 - Robust
 - Low-cost

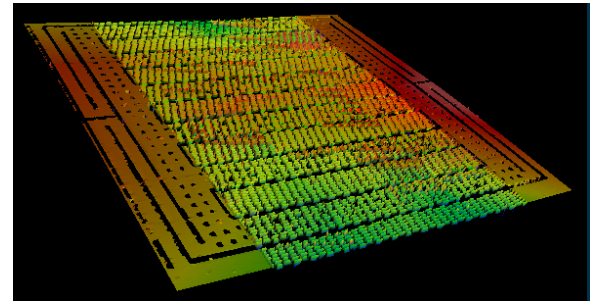
- When used with wider grating elements, for diffraction order $M=6$, the neighboring diffraction orders come closer...



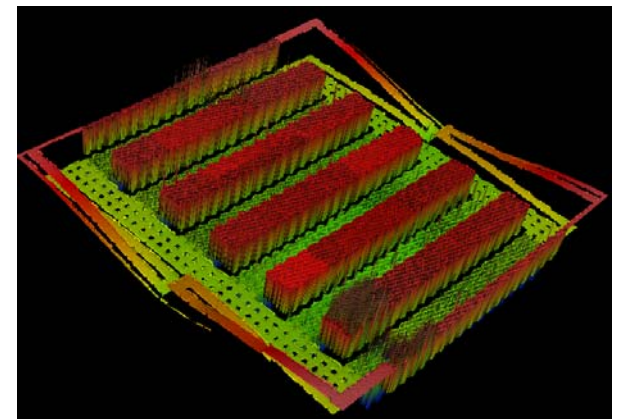
Actuation characteristic



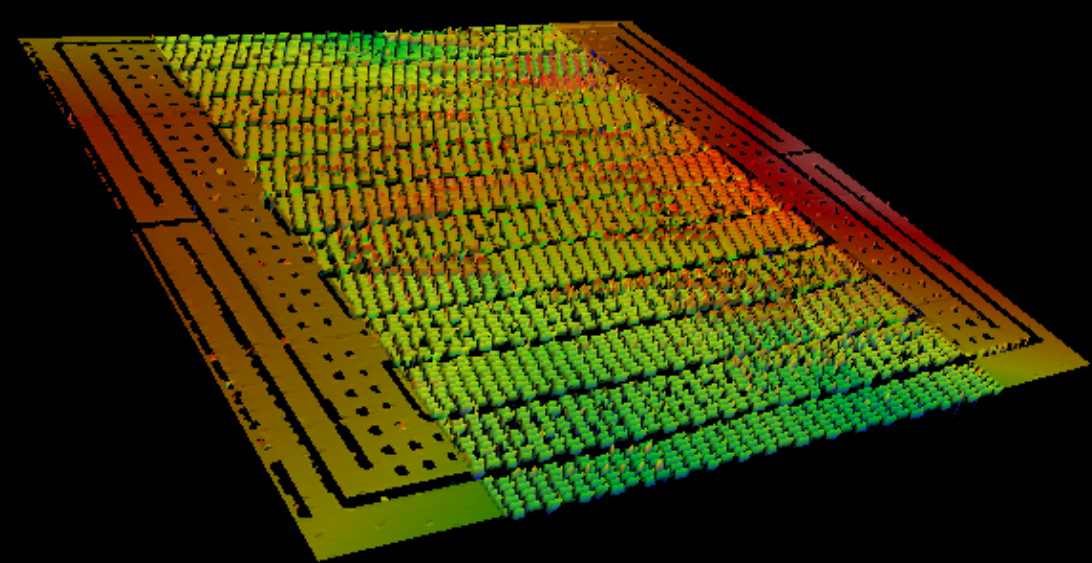
- Bistable operation with snap-down at 4.2V
- Hysteresis due to pull-in effect



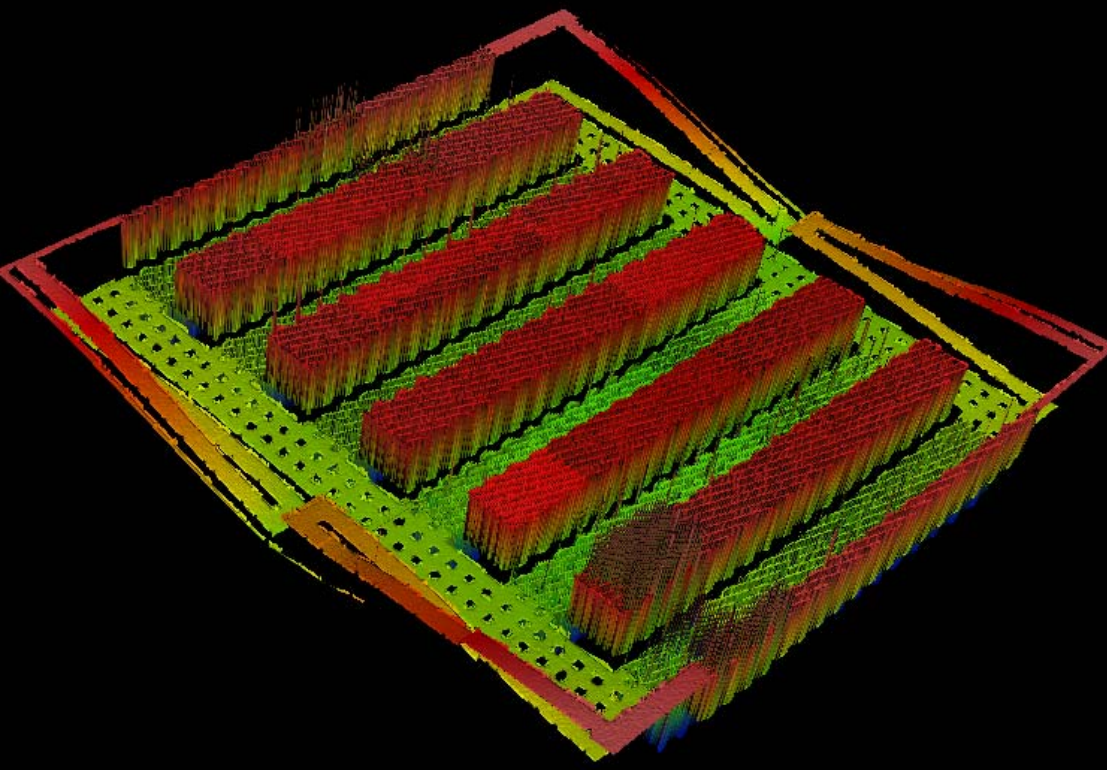
Idle (0V)



Fully actuated (5V)

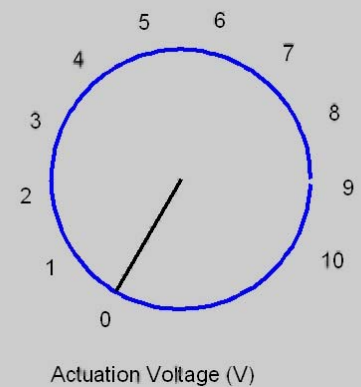
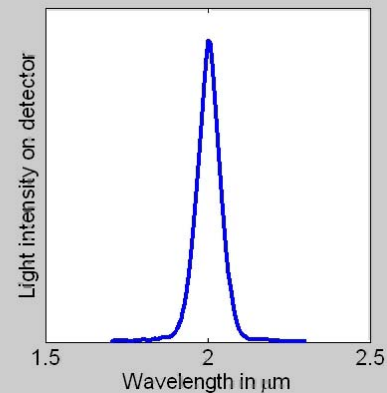
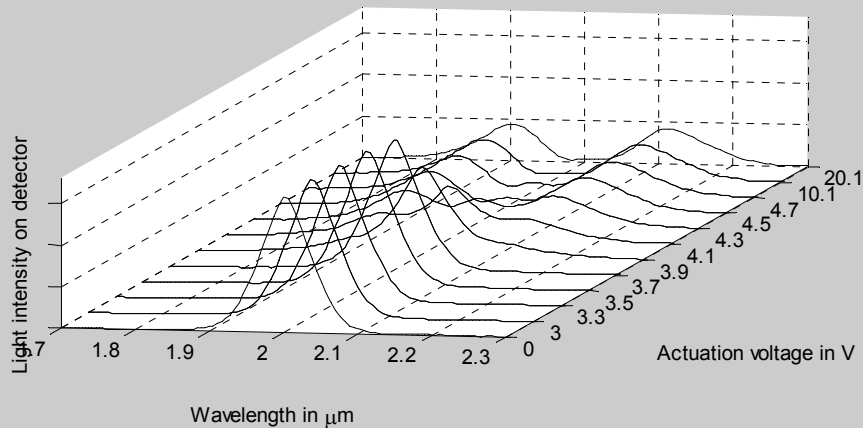
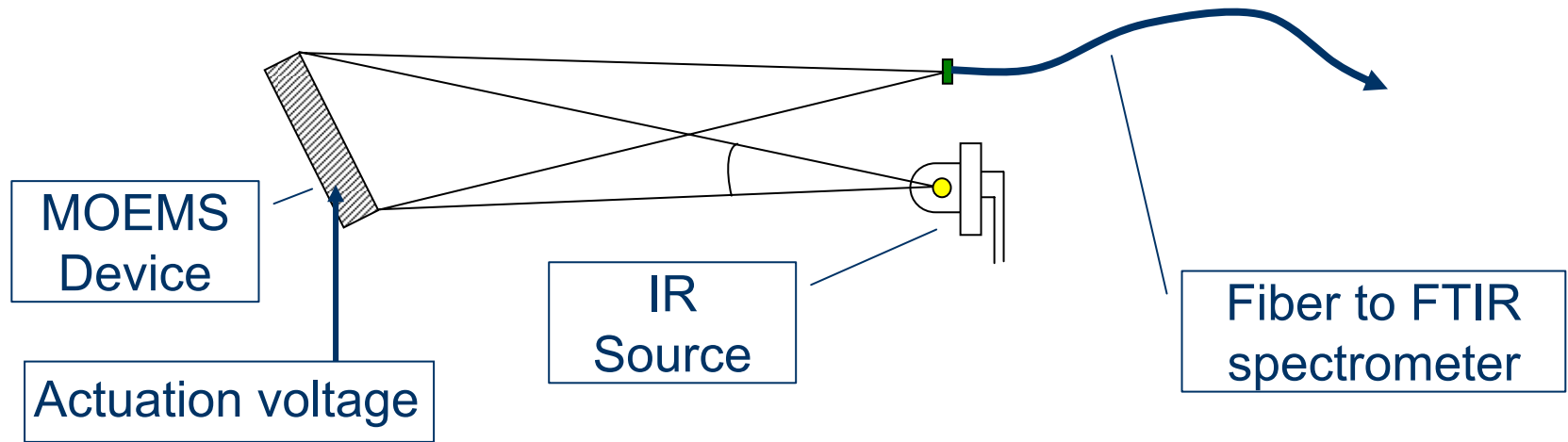


0V



5V

Infrared spectral characterization



”Grating light valves” for displacement sensing (F.L. Degertekin)

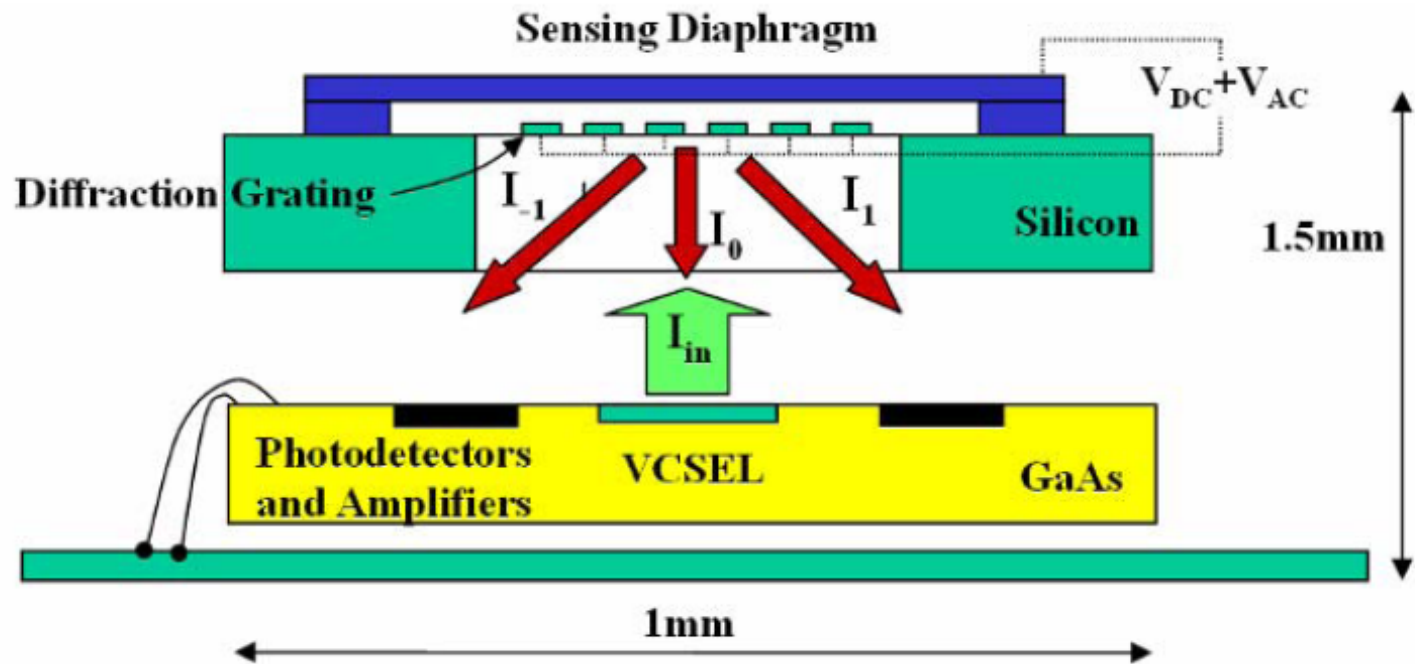


Fig. 1. Schematic of the optical displacement detection scheme. Light from the VCSEL is modulated by the diffraction grating and the reflector providing the same interference behavior and sensitivity as a Michelson interferometer. For a microphone, the top reflector is a rigidly supported membrane.

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Fig. 2. Experimentally traced interference curve using a VCSEL as the light source [11]

